19-3995; Rev 0; 3/06

EVALUATION KIT AVAILABLE

# Low VBATT, 20µA IQ, 1MHz Synchronous Boost Converter with True Shutdown

# **\_General Description**

The MAX8627 step-up converter is a high-efficiency, low-quiescent current, synchronous boost converter with True Shutdown<sup>™</sup> and inrush current limiting. The MAX8627 generates any boosted output voltage from 3V to 5V from either a 2-cell NiMH/NiCd or a single-cell Li+/Li polymer battery.

Quiescent current is only 20µA (typ), and at light loads the converter pulses only as needed for best efficiency. At higher loads, PWM mode maintains fixed 1MHz operation for lowest noise and ripple.

The MAX8627 includes an internal soft-start to limit inrush current to a maximum of 500mA. Additional features include True Shutdown, internal compensation, and adjustable current limit. The MAX8627 is available in a tiny 3mm x 3mm TDFN package and is ideal for use in handheld devices such as DSCs, PDAs, and smartphones.

## Applications

DSC Motors and Backup Power Microprocessor/DSP Core Power Cellphones, PDAs, MP3 Players Portable Handheld Devices

True Shutdown is a trademark of Maxim Integrated Products, Inc.

# **Typical Operating Circuit**



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\_Features

- 1MHz PWM Switching Frequency
- True Shutdown Output
- Up to 95% Efficiency
- ♦ 1.0A Guaranteed Output Current
- ♦ Soft-Start Eliminates Inrush Current
- ♦ 20µA (typ) Quiescent Current
- ♦ 0.1µA Logic-Controlled Shutdown
- Internal Synchronous Rectifier
- Internal Compensation
- Adjustable Current Limit
- Low-Noise Antiringing Feature
- Tiny 14-Pin, 3mm x 3mm, TDFN Package

PART	PIN- PACKAGE	PKG CODE	TOP MARK
MAX8627ETD+	14 TDFN-EP* 3mm x 3mm	T1433-2	AAQ

**Note:** The device operates in the -40°C to +85°C extended operating temperature range.

\*EP = Exposed pad. +Denotes lead-free package.

# Pin Configuration

**Ordering Information** 



Maxim Integrated Products 1

For pricing, delivery, and ordering information, please contact Maxim/Dallas Direct! at 1-888-629-4642, or visit Maxim's website at www.maxim-ic.com.

# **ABSOLUTE MAXIMUM RATINGS**

OUTS, BATT to GND	0.3V to +6V
LX Current (Note 1)	3.5A
AGND, PG to GND	0.3V to +0.3V
POUT to OUTS	0.3V to +0.3V
FB, ILIM, ON to	
GND0.3V to the higher of (VOUTS +	0.3V) and (V <sub>BATT</sub> + 0.3V)

Continuous Power Dissipation ( $T_A = +70^{\circ}C$ )
14-Pin TDFN 3mm x 3mm
(derate 18.2mW/°C above +70°C)1454mW
Operating Temperature Range40°C to +85°C
Junction Temperature+150°C
Storage Temperature Range65°C to +150°C
Lead Temperature (soldering, 10s)+300°C

**Note 1:** LX has internal clamp diodes to the IC internal power node V<sub>PWR</sub> (where V<sub>PWR</sub> is the higher of BATT or POUT) and PG. Applications that forward bias these diodes should take care not to exceed the device's power-dissipation limits.

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## **ELECTRICAL CHARACTERISTICS**

(Vouts = VPout = 5V, Von = VBATT = 3.6V, VILIM = GND, TA = -40°C to +85°C, typical values are at TA = +25°C, unless otherwise noted.)

PARAMETER	CONDI	TIONS	MIN	ТҮР	MAX	UNITS	
GENERAL	·		•				
Operating Input Voltage Range	(Note 1)		0.9		5.5	V	
Minimum Startup Voltage	No load (Note 1)			1.2	1.5	V	
Maximum Startup Current Limit				0.5		А	
	Shutdown, ON = GND	$T_A = +25^{\circ}C$		0.1	1		
		T <sub>A</sub> = +85°C		0.2			
Supply Current	No lood no switching	$T_A = 0^{\circ}C \text{ to } +85^{\circ}C$		20	30	μA	
	No load, no switching	T <sub>A</sub> = -40°C (Note 2)		20	35		
	No load, switching			20			
OSCILLATOR							
Switching Frequency			0.95	1.0	1.05	MHz	
Startup Switching Frequency				2.0		MHz	
Maximum Duty Cycle			82.5	87.0		%	
Output Voltage Adjust Range			3.0		5.2	V	
FB Regulation Voltage	No load		1.005	1.015	1.025	V	
FB Load Regulation	0A to 1A output current load	step		-30		mV/A	
FB Line Regulation	VBATT = 2.7V to 3V, output c	urrent = 0.5A		+20		mV	
FB Input Leakage Current	V <sub>FB</sub> = 1.2V,	$T_A = +25^{\circ}C$	-50	-10	+50	nA	
FB Input Leakage Current	VOUTS = VPOUT = VBATT = 5	.5V T <sub>A</sub> = +85°C		-10		ΠA	
ILIM Dual Mode™ Threshold	Low level				0.25	V	
	High level		0.45			v	
Idle Mode Trip Level	(Note 3)			50		mA	
DC-DC SWITCHES							
n-Channel On-Resistance				0.15	0.25	Ω	
p-Channel On-Resistance				0.15	0.25	Ω	
Damping Switch On-Resistance				17	30	Ω	
n-Channel Current limit	$V_{ILIM} = 0V$		3.2	3.5	3.7	А	
	$V_{ILIM} = 0.6V$			1.0		A	

Dual Mode is a trademark of Maxim Integrated Products, Inc.



# **ELECTRICAL CHARACTERISTICS (continued)**

(V<sub>OUTS</sub> = V<sub>POUT</sub> = 5V, V<sub>ON</sub> = V<sub>BATT</sub> = 3.6V, V<sub>ILIM</sub> = GND, T<sub>A</sub> = -40°C to +85°C, typical values are at T<sub>A</sub> = +25°C, unless otherwise noted.)

PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
p-Channel Turn-Off Current				10		mA
		$T_A = +25^{\circ}C$		0.1	1	
POUT Leakage Current	$V_{LX} = 0V, V_{POUT} = V_{BATT} = 5.5V$	$T_A = +85^{\circ}C$		0.2		μA
	$V_{LX} = 0V$ and $V_{POUT} = 5.5V$ or $V_{LX} =$	$T_A = +25^{\circ}C$		0.1	1	
LX Leakage Current	5.5V and $V_{OUTS} = V_{POUT} = 0V$	$T_A = +85^{\circ}C$		0.2		μA
Soft-Start Interval	Output current = 0.5A			5.25		ms
Overload Protection Fault Delay				65		ms
LOGIC INPUTS						
ON Input Low Level	1.5V < VPOUT = VOUTS = VBATT ≤ 1.8V	/			0.2	v
	$1.8V < V_{POUT} = V_{OUTS} = V_{BATT} \le 5.5V_{POUT}$	/			0.5	v
ON Input High Level	1.5V < VPOUT = VOUTS = VBATT ≤ 1.8V	1	V <sub>POUT</sub> - 0.2			V
	1.8V < VPOUT = VOUTS + VBATT ≤ 5.5V	/	1.6			
	Vouts = Vpout = Vbatt = 5.5V,	$T_A = +25^{\circ}C$		0.01	1	
ON, Input Leakage Current	ON = OV  or  ON = 5.5V	$T_A = +85^{\circ}C$		0.02		μA
Thermal Shutdown				+160		°C

Note 1: The MAX8627 is powered from OUTS. Once started, the IC operates down to 0.9V.

**Note 2:** Specifications to -40°C are guaranteed by design and not production tested.

**Note 3:** The idle-mode current threshold is the transition point between fixed-frequency PWM operation and idle-mode operation. The specification is given in terms of output load current for an inductor value of 1µH. For a step-up converter, the idlemode transition varies with the input-to-output voltage ratio.

**Typical Operating Characteristics** 

(Circuit of Figure 1, V<sub>OUTS</sub> = V<sub>POUT</sub> = 5V, V<sub>ON</sub> = V<sub>BATT</sub> = 3.6V,  $T_A$  = +25°C, unless otherwise noted.)

**EFFICIENCY vs. LOAD CURRENT EFFICIENCY vs. LOAD CURRENT** MAXIMUM LOAD CURRENT WITH 5V OUTPUT WITH 3.3V OUTPUT vs. INPUT VOLTAGE 100 3.5 100 = 3.0V= 4 2 V VBATT 90 90 3.0 80 80 Ð MAXIMUM LOAD CURRENT 25 70 70  $V_{POUT} = 3.3 \dot{V}$ V<sub>BATT</sub> = 3.6V EFFICIENCY (%) EFFICIENCY (%) 60 1.8V 60 2.0 V<sub>BATT</sub> 3 OV = 1.5\ VRATT 50 50  $V_{BATT} = 2.4V$ 1.5 40 40  $V_{BATT} = 1.8V$ 30 30 1.0  $V_{POUT} = 5V$ 20 20 0.5 10 10 0 0 0 0.01 0.1 1 10 100 1000 0.01 0.1 1 10 100 1000 1.0 2.0 3.0 4.0 5.0 LOAD CURRENT (mA) LOAD CURRENT (mA) INPUT VOLTAGE (V) **NO-LOAD INPUT CURRENT NO-LOAD INPUT CURRENT** vs. INPUT VOLTAGE WITH 3.3V OUTPUT vs. INPUT VOLTAGE WITH 5V OUTPUT **OUTPUT VOLTAGE vs. LOAD CURRENT** 90 180 5.12  $R1 = 1.15M\Omega$ ,  $R2 = 499k\Omega$  $R1 = 2M\Omega$ ,  $R2 = 499k\Omega$ 5 10 80 160 OUTPUT ONLY LOADED WITH THE FB OUTPUT ONLY LOADED WITH THE FB RESISTOR-DIVIDER NETWORK. RESISTOR-DIVIDER NETWORK. 5.08 70 140 V<sub>BATT</sub> = 4.2V () 5.06 5.04 5.02 5.00 4.98  $T_A = +85^{\circ}C$ NPUT CURRENT (mA) NPUT CURRENT (mA) 60 120 T∧ = +85<sup>°</sup>C V<sub>BATT</sub> = 3.6V ÎHH 50 100 VBATT = 3.0V 40 80 V<sub>BATT</sub> = 2.4V VBATT 30 .8\ 60  $T_A = +25^{\circ}C$ 20 40 +25°C 4.96 10 20  $T_A = 40^{\circ}C$  $T_A = 40^{\circ}C$ 4.94 4.92 0 0 0.1 1000 1.0 1.5 2.0 2.5 3.0 3.5 2 5 0.01 10 100 1 3 1 4 LOAD CURRENT (mA) INPUT VOLTAGE (V) INPUT VOLTAGE (V) SHUTDOWN CURRENT **STARTUP VOLTAGE vs. LOAD CURRENT** vs. INPUT VOLTAGE WITH 5V OUTPUT **SOFT-START TIME vs. LOAD CURRENT** 700 3.0 6 600 2.5 5  $T_A = +25^{\circ}C$ SHUTDOWN CURRENT (nA) 500 STARTUP VOLTAGE (V) SOFT-START TIME (ms) 2.0 4  $T_A = +85^{\circ}C$ 400 1.5 3 300 1.0 2  $T_A = 40^{\circ}C$ 200  $T_A = +25^{\circ}C$  $T_A = +85^{\circ}C$  $T_A = 40^{\circ}C$ 0.5 100 1 0 0 0 5.5 1000 1.5 2.5 3.5 4.5 0 200 400 600 800 0 0.1 0.2 0.3 0.4 0.5

LOAD CURRENT (mA)

LOAD CURRENT (A)

INPUT VOLTAGE (V)

# **Typical Operating Characteristics (continued)**

(Circuit of Figure 1, V<sub>OUTS</sub> = V<sub>POUT</sub> = 5V, V<sub>ON</sub> = V<sub>BATT</sub> = 3.6V, T<sub>A</sub> = +25°C, unless otherwise noted.)









LIGHT-LOAD SWITCHING WAVEFORMS





M/X/M

# **Typical Operating Characteristics (continued)**

(Circuit of Figure 1, V<sub>OUTS</sub> = V<sub>POUT</sub> = 5V, V<sub>ON</sub> = V<sub>BATT</sub> = 3.6V, T<sub>A</sub> = +25°C, unless otherwise noted.)



SWITCHING FREQUENCY vs. TEMPERATURE





BODE PLOT WITH 2 x 22µF CERAMIC



BODE PLOT WITH 2 x 47 $\mu$ F TANTALUM OUTPUT CAPACITORS (130m $\Omega$  ESR), 500mA LOAD



# \_Pin Description

PIN	NAME	FUNCTION
1	GND	Analog Ground. Connect to PG and AGND.
2	FB	Voltage Feedback Input. Connect FB to the center of an external feedback network between OUTS and GND (see the <i>Setting the Output Voltage</i> section). FB regulates to 1.015V (typ).
3	ON	Active-High Enable Input. Connect ON to BATT or logic high for normal operation. Connect ON to GND or logic low for True Shutdown mode.
4, 5	BATT	Supply Voltage Input. Connect to the battery or a supply from 1.5V to 5.5V. Connect two $22\mu F$ ceramic capacitors from BATT to PG.
6, 7	POUT	Power Output. Connect two 22µF ceramic capacitors from POUT to PG (see the <i>Capacitor Selection</i> section).
8, 9	LX	Inductor Connection. LX is high impedance in shutdown.
10, 11	PG	Power Ground. Connect to GND and AGND.
12	AGND	Analog Ground. Connect to GND and PG.
13	ILIM	n-Channel Current-Limit Control. For the maximum current limit of 3.5A, connect ILIM to GND. For lower current-limit settings, connect ILIM to a resistor-divider from POUT to GND (see the <i>Setting the Current Limit</i> section).
14	OUTS	IC Power Input. Supplied from the output. Connect OUTS to POUT.
_	EP	Exposed Pad. Connect EP to GND. This does not remove the requirement for a proper ground connection to GND.



Figure 1. Typical Applications Circuit with an Adjustable Output Voltage and Adjustable Current Limit





## **Detailed Description**

The MAX8627 is a current-mode step-up converter that uses a fixed-frequency PWM architecture with True Shutdown. Consuming only 20 $\mu$ A of quiescent current, the MAX8627 is highly efficient, with an internal switch and synchronous rectifier. Shutdown reduces the quiescent current to less than 1 $\mu$ A. Low quiescent current and low noise make this device ideal for powering portable equipment.

The MAX8627 step-up DC-to-DC switching converter typically generates a 3V to 5V output voltage from a 1.5V to 4.2V battery input voltage. The IC operates in bootstrapped mode with the output powering the IC once the output voltage is equal to, or exceeds, 2.7V. The default current limit is set at 3.5A to deliver 1A at 5V with an Li+ battery, or 500mA at 5V using a 2-cell NiCd/NiMH battery. The current limit may be lowered using an external resistor at ILIM to allow for smaller components in lower power applications. Internal soft-start limits the inrush current to less than 500mA under no-load conditions during startup.

The MAX8627 switches at an internally set frequency of 1MHz allowing for tiny external components. Internal compensation further reduces the external component count in cost and space-sensitive applications. The MAX8627 is optimized for use in DSC and other applications requiring low quiescent current for maximum battery life. Figure 1 shows the typical applications circuit. Figure 2 gives the functional diagram.

## **DC-DC Converter**

The MAX8627 uses a current-mode PWM control scheme. The voltage difference between FB and an internal 1.01V reference generates an error signal that programs the peak inductor current to regulate the output voltage. The default peak inductor current limit is typically 3.5A. Inductor current is sensed across the internal switch and summed with a slope-compensation signal. The PWM comparator compares this summed signal to the error amplifier output. At the beginning of each clock cycle, the n-channel switch turns on until the PWM comparator trips. During this time, inductor current ramps up, storing energy in its magnetic field. When the n-channel switch turns off, the internal synchronous p-channel rectifier turns on. The inductor releases the stored energy as the current ramps down and provides energy to the output.

The device operates in PWM when driving medium to heavy loads. As the load current decreases and crosses the low-power idle mode threshold, the PWM comparator and oscillator are disabled. In this low-power idle mode, switching occurs only as needed to service the output. This improves the efficiency for light loads and the IC consumes only  $20\mu$ A under no-load conditions. At light loads, the output ripple has a frequency component that varies with load current. The threshold for entering the low-power mode is determined by sensing the voltage drop across the internal switch and comparing it to an internally generated reference level. This threshold is approximately 50mA with a 3.6V input and 5V output.

When switching in low-power mode, the inductor current terminates at zero for each switching cycle. When operating in this manner, the inductor current is called discontinuous. In older DC-DC converters, radiated noise may be higher when inductor current is discontinuous, because of ringing at the LX switch. The MAX8627 features an internal damping switch to minimize ringing at LX when inductor current is discontinuous. The damping switch places an impedance across the inductor and supplies a path to dissipate the resonant energy in the inductor and capacitor to damp the ringing at the LX. The damping switch has little effect on output voltage ripple but does reduce EMI.

At higher loads, the MAX8627 operates in PWM mode. Regulation is achieved by modulating the MOSFET switch pulse to control the amount of power transferred per cycle. Switching harmonics generated by fixedfrequency operation are consistent and easily filtered. This is important in noise-sensitive applications.

## Load-Transient Response/Voltage Positioning

The MAX8627 matches the load regulation to the voltage droop seen during load transients. This is sometimes called voltage positioning. Benefits include lower peak-to-peak output-voltage deviation for a given load step without requiring an increase in filter load capacitance. There is minimal voltage droop when transitioning from a light load to full load and minimum overshoot when going from full load to light load.

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The term "positioning" refers to setting the output voltage to a level that is dependent on load current (see Figure 3). At minimum load, the output voltage is set to a slightly higher than nominal level. At full load, the output voltage is slightly lower than the nominal level. With voltage positioning, the total voltage deviation during a transient is significantly improved over traditional highgain control loops. Traditional high-gain loops use integrators that maximize gain at low frequencies to provide tight DC-load regulation; however, due to the capacitive element in the feedback loop, these highgain amplifiers typically take hundreds of microseconds to respond to a load step and return to steady state. As a result, the voltage can droop by as much as 6% or more during the recovery time. In portable equipment where the output load can change frequently, and the amount of output capacitance that can fit is limited. this can result in a wide short-term output fluctuation (see Figure 4).

Voltage positioning on the MAX8627 allows up to 3% (typ) of load regulation and no further transient droop (Figures 3 and 4). Thus, during load transients the voltage delivered remains within specification more effectively than other regulators that might have tighter DC accuracy. In systems with high-speed CPUs, thousands of system clock cycles can occur during the time it takes a traditional high-gain loop to respond to a load step. Consequently, 3% load regulation with no transient droop is better suited to such systems than a power supply that may spec 1% DC load regulation, but then exhibits 6% or more of transient droop during load steps (see the Load Transient Response in the *Typical Operating Characteristics* section).

## **True Shutdown**

Connecting ON to GND or logic low places the MAX8627 in shutdown mode and reduces supply current to  $0.1\mu$ A. In shutdown, the control circuitry, internal switching MOSFET, and synchronous rectifier turn off and LX becomes high impedance. Connect ON to BATT or logic high for normal operation.

The MAX8627 has an internal synchronous rectifier, which allows for conversion efficiencies as high as 95%. In conventional boost circuits, the body diode of the synchronous rectifier is forward biased in shutdown and allows current flow from the battery to the output. If the load cannot be shut down, an external switch is required to avoid depleting the battery during shutdown. A proprietary design in the MAX8627 allows the synchronous rectifier to provide True Shutdown with no additional components. This allows the output to fall to GND in shutdown and removes any connection between the input and output.

## Soft-Start

The MAX8627 has internal soft-start circuitry that eliminates inrush current at startup, reducing transients on the input source. Soft-start is particularly useful for higher impedance input sources, such as Li+ and alkaline cells. The soft-start duration is proportional to the size of the output capacitor and load resistance with a typical time of 5.25ms. See the *Typical Operating Characteristics* section for plots of Soft-Start Time vs. Load Current and Soft-Start Time vs. Input Voltage. Inrush current is controlled during startup and initially set to 500mA. After 1000 clock cycles, if the output voltage is not within regulation, the startup current limit is



Figure 3. Load-Regulation Specification



Figure 4. Transient-Response Comparison



incremented by 230mA. If after 13 increments, the output is still not in regulation, the MAX8627 latches off, assuming a short-circuit overload condition exists on the output. To clear the latched condition, cycle ON.

## **Fault Protection**

The MAX8627 has a fault-overload protection. After soft-start, the device is set to detect an out-of-regulation state that could be caused by an overload. If the output remains faulted for 65ms, then the MAX8627 latches off. Fault-detection circuitry is disabled during soft-start. If short on the output exists before the MAX8627 is turned ON, the converter completes the soft-start sequence and latches off. The converter can be reinitialized from a fault latch-off state by toggling the ON pin or by cycling the input power.

## **BATT/Damping Switch**

The MAX8627 features an internal damping switch to minimize ringing at LX caused by the resonant circuit formed by the inductor and output capacitor in discontinuous conduction mode. This occurs at light loads. The damping switch connects across the inductor when the inductor energy is depleted and supplies a path to dissipate the resonant energy. Damping LX ringing does not change the output ripple but reduces EMI.

# Applications Information

## **Setting the Output Voltage**

To set the output voltage to between 3V and 5V, connect FB to the center of an external resistor voltagedivider between OUTS and GND, as shown in Figure 1. Select the value of R2 less than  $500k\Omega$ , and then calculate the value for R1 as follows:

$$R1 = R2 x \left(\frac{V_{OUT}}{V_{FB}} - 1\right)$$

where V<sub>FB</sub> is the FB regulation voltage, 1.015V (typ).

## **Inductor Selection**

In most step-up converter designs, a reasonable inductor value can be derived from the following equation,

 Table 1. Recommended Inductors

which sets peak-to-peak inductor current at 1/2 the DC inductor current:

$$L = \frac{2 \times V_{BATT} \times D \times (1-D)}{I_{OUT(MAX)} \times f_{SW}}$$

where  $f_{SW}$  is the switching frequency (1MHz), and D is the duty factor given by D = 1 - (V<sub>BATT</sub> / V<sub>OUT</sub>).

Using L from the equation above results in a peak-topeak inductor current ripple of  $0.5 \times I_{OUT}$  / (1 - D), and a peak inductor current of  $1.25 \times I_{OUT}$  / (1 - D). Ensure the peak (saturation) current rating of the inductor meets or exceeds this requirement.

The recommended inductance range for the MAX8627 is  $1\mu$ H to  $4.7\mu$ H. See Table 1 for recommended inductors.

## **Capacitor Selection**

## **Output Capacitor**

Output capacitors C3 and C4 in Figure 1 are required to keep the output voltage ripple small and to ensure regulation loop stability. The output capacitors must have low impedance at the switching frequency. Ceramic capacitors are highly recommended due to their small size and low ESR. Make sure the output capacitors maintain their capacitance over DC bias and the desired operating temperature characteristics generally perform well. Two 22 $\mu$ F ceramic capacitors in parallel are recommended. Alternatively, two 47 $\mu$ F tantalum capacitors with 70m $\Omega$  or lower ESR may be used.

## Input Capacitor

Input capacitors C1 and C2 reduce the current peaks drawn from the battery or input power source and reduce switching noise in the IC. The impedance of the input capacitors at the switching frequency should be kept very low. Ceramic capacitors are highly recommended due to their small size and low ESR. Make sure the input capacitors maintain their capacitance over DC bias and the desired operating temperature range. Ceramic capacitors with X5R or X7R temperature characteristics generally perform well. Two 22µF ceramic capacitors are recommended.

PART	INDUCTANCE (µH)	RATED CURRENT (mA)	SIZE: L (mm, typ) x W (mm, typ) x H (mm, max)
TOKO A918CY	1.0	3500	6.3 x 6.2 x 2
TOKO A997AS	1.5	2150	3.8 x 3.8 x 1.8

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## **Setting the Current Limit**

ILIM sets the current limit when the output reaches regulation. It is different from the startup current limit used during soft-start to control inrush current. For the maximum current limit of 3.5A, connect ILIM to GND. To set the current limit (ILIM) lower than 3.5A, connect ILIM to a resistor-divider from POUT to GND as shown in Figure 1. Note, however, that the idle-mode threshold does not change with voltage setting on ILIM.

Set R3 between  $30k\Omega$  and  $300k\Omega$ , then calculate the value of R4 as follows:

$$R4 = R3 \times \left(\frac{V_{POUT}}{(I_{LIM} + 0.64A) \times 0.2865\Omega} - 1\right)$$

## **PC** Board Layout and Routing

Good PC board layout is important to achieve optimal performance from the MAX8627. Poor design can cause excessive conducted and/or radiated noise. Conductors carrying discontinuous currents and any high-current path should be made as short and wide as possible. Keep the feedback network (R1 and R2) very close to the IC, preferably within 0.2in of the FB and GND pins. Nodes with high dV/dt (switching nodes) should be kept as small as possible and routed away from FB. Connect the input and output capacitors as close as possible to the IC. Refer to the MAX8627 evaluation kit for a PC board layout example.

## **Chip Information**

PROCESS: BICMOS

# **Package Information**

(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information go to **www.maxim-ic.com/packages**.)



# Package Information (continued)

(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information go to **www.maxim-ic.com/packages**.)

COMMON		SIONS		PACKAGE V	ARIAT	IONS						
SYMBOL	MIN.	MAX.		PKG. CODE	N	D2	E2	е	JEDEC SPEC	b	[(N/2)-1] x e	
А	0.70	0.80		T633-1	6	1.50±0.10	2.30±0.10	0.95 BSC	MO229/WEEA	0.40±0.05	1.90 REF	1
D	2.90	3.10		T633-2	6	1.50±0.10	2.30±0.10	0.95 BSC	MO229/WEEA	0.40±0.05	1.90 REF	1
E	2.90	3.10		T833-1	8	1.50±0.10	2.30±0.10	0.65 BSC	MO229 / WEEC	0.30±0.05	1.95 REF	1
A1	0.00	0.05		T833-2	8	1.50±0.10	2.30±0.10	0.65 BSC	MO229 / WEEC	0.30±0.05	1.95 REF	1
L	0.20	0.40		T833-3	8	1.50±0.10	2.30±0.10	0.65 BSC	MO229 / WEEC	0.30±0.05	1.95 REF	1
k	0.25	MIN.		T1033-1	10	1.50±0.10	2.30±0.10	0.50 BSC	MO229 / WEED-3	0.25±0.05	2.00 REF	1
A2	0.20	REF.		T1033-2	10	1.50±0.10	2.30±0.10	0.50 BSC	MO229 / WEED-3	0.25±0.05	2.00 REF	
				T1433-1	14	1.70±0.10	2.30±0.10	0.40 BSC		0.20±0.05	2.40 REF	
				T1433-2	14	1.70±0.10	2.30±0.10	0.40 BSC		0.20±0.05	2.40 REF	1
									L		2.101121	J
2. COPL 3. WARP 4. PACK 5. DRAW 6. "N" 1 7. NUME	ANARITY AGE SH AGE LE ING CO S THE BER OF	' Shall Iall No Ngth/P Nforms Total N Leads	NOT EX T EXCEE ACKAGE TO JED IUMBER SHOWN	. ANGLES IN DEED 0.08 m D 0.10 mm. WIDTH ARE Cd EC M0229, E DF LEADS. ARE FOR REF RIENTATION F	m. DNSID XCEP EREN	ERED AS S T DIMENSIO CE ONLY.	NS "D2" AN		C(S). ID T1433—1 & T <sup>1</sup>		2.101121	I

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