19-1006; Rev 4; 4/09

EVALUATION KIT AVAILABLE

High-Efficiency, Seamless Transition, Step-Up/Down DC-DC Converter

General Description

The MAX8625A PWM step-up/down regulator is intended to power digital logic, hard disk drives, motors, and other loads in portable, battery-powered devices such as PDAs, cell phones, digital still cameras (DSCs), and MP3 players. The MAX8625A provides either a fixed 3.3V or adjustable output voltage (1.25V to 4V) at up to 0.8A from a 2.5V to 5.5V input. The MAX8625A utilizes a 2A peak current limit.

Maxim's proprietary H-bridge topology provides a seamless transition through all operating modes without the glitches commonly seen with other devices. Four internal MOSFETs (two switches and two synchronous rectifiers) with internal compensation minimize external components. A SKIP input selects a low-noise, fixed-frequency PWM mode, or a high-efficiency skip mode where the converter automatically switches to PFM mode under light loads for best light-load efficiency. The internal oscillator operates at 1MHz to allow for a small external inductor and capacitors.

The MAX8625A features current-limit circuitry that shuts down the IC in the event of an output overload. In addition, soft-start circuitry reduces inrush current during startup. The IC also features True Shutdown[™], which disconnects the output from the input when the IC is disabled. The MAX8625A is available in a 3mm x 3mm, 14-pin TDFN package.

Applications

PDAs and Smartphones

DSCs and Camcorders

MP3 Players and Cellular Phones

Battery-Powered Hard Disk Drive (HDD)

Pin Configuration



True Shutdown is a trademark of Maxim Integrated Products, Inc.

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For pricing, delivery, and ordering information, please contact Maxim Direct at 1-888-629-4642, or visit Maxim's website at www.maxim-ic.com.

Features

Four Internal MOSFET True H-Bridge Buck/Boost

- Glitch-Free, Buck-Boost Transitions
- Minimal Output Ripple Variation on Transitions
- Up to 92% Efficiency
- ♦ 37µA (typ) Quiescent Current in Skip Mode
- ♦ 2.5V to 5.5V Input Range
- Fixed 3.3V or Adjustable Output
- ♦ 1µA (max) Logic-Controlled Shutdown
- True Shutdown
- Output Overload Protection
- Internal Compensation
- Internal Soft-Start
- 1MHz Switching Frequency
- ♦ Thermal-Overload Protection
- Small 3mm x 3mm, 14-Pin TDFN Package

Ordering Information

PART	PIN- PACKAGE	TOP MARK
MAX8625AETD+	14 TDFN-EP**	ABQ

Note: The device is specified over the -40°C to +85°C extended temperature range.

+Denotes a lead(Pb)-free/RoHS-compliant package.

**EP = Exposed pad.

_Typical Operating Circuit



ABSOLUTE MAXIMUM RATINGS

IN, OUT, SKIP, ON to GND	0.3V to +6V
REF, FB to GND	
LX2, LX1 (Note 1)	±1.5A _{RMS}
Continuous Power Dissipation ($T_A = +70^{\circ}C$)
Single-Layer Board (derate 18.5mW/°C	
above $T_A = +70^{\circ}C$)	1482mW

Operating Temperature Range	40°C to +85°C
Junction Temperature	+150°C
Storage Temperature Range	65°C to +150°C
Lead Temperature (soldering, 10s)	+300°C

Note 1: LX1 and LX2 have internal clamp diodes to IN, GND and OUT, GND, respectively. Applications that forward bias these diodes should take care not to exceed the device's power-dissipation limits.

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

ELECTRICAL CHARACTERISTICS

 $(V_{IN} = 3.6V, ON = \overline{SKIP} = IN, FB = GND, V_{OUT} = 3.3V, LX_unconnected, C_{REF} = C5 = 0.1\mu F to GND, Figure 4. T_A = -40°C to +85°C. Typical values are at T_A = +25°C, unless otherwise noted.) (Note 2)$

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Supply Range	VIN		2.5		5.5	V
UVLO Threshold	UVLO	V _{IN} rising, 60mV hysteresis	2.20		2.49	V
Quiescent Supply Current, FPWM Mode, Switching	I _{IN}	No load, V _{OUT} = 3.2V		15	22	mA
Quiescent Supply Current, Skip Mode, Switching	l _{IN}	$\overline{\text{SKIP}}$ = GND, no load		37		μA
Quiescent Supply Current, No Switching, Skip Mode	l _{IN}	$\overline{\text{SKIP}}$ = GND, FB = 1.3V		35	45	μA
		$ON = GND$, $T_A = +25^{\circ}C$		0.1	1	
Shutdown Supply Current	IIN	T _A = +85°C		0.2		μA
		PWM mode, V _{IN} = 2.5V to 5.5V		3.30		V
Output Voltage Accuracy		$I_{OUT} = 0$ to 0.5A, $V_{IN} = 2.5V$ to 5.5V, T _A = -40°C to +85°C (Note 3)	-1		+1	%
(Fixed Output)		SKIP mode, valley regulation value		3.28		V
		Average skip voltage		3.285		
		Load step +0.5A		-3		%
Output Voltage Range (Adjustable Output)			1.25		4.00	V
Maximum Output Current		V _{IN} = 3.6V		0.80		А
Soft-Start		$L = 3.3\mu$ H; $C_{OUT} = C3 + C4 = 44\mu$ F		250		mA/ms
Load Regulation		I _{OUT} = 0 to 500mA		0.1		%/A
Line Regulation		V _{IN} = 2.5V to 5.5V		0.03		%/V
OUT Bias Current	IOUT	V _{OUT} = 3.3V		3		μA
REF Output Voltage	V _{REF}	V _{IN} = 2.5V to 5.5V	1.244	1.25	1.256	V
REF Load Regulation		I _{REF} = 10μA		1		mV
FB Feedback Threshold	V _{FB}	I_{OUT} = 0 to full load, PWM mode; V_{IN} = 2.5V to 5.5V	1.244	1.25	1.258	V



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ELECTRICAL CHARACTERISTICS (continued)

 $(V_{IN} = 3.6V, ON = \overline{SKIP} = IN, FB = GND, V_{OUT} = 3.3V, LX_unconnected, C_{REF} = C5 = 0.1\mu F to GND, Figure 4. T_A = -40°C to +85°C. Typical values are at T_A = +25°C, unless otherwise noted.) (Note 2)$

PARAMETER	SYMBOL	CONDITIONS	MIN	ТҮР	MAX	UNITS	
FB Dual-Mode Threshold	VFBDM		75	100	125	mV	
FR Lookage Current	les	V _{FB} = 1.3V, T _A = +25°C		0.001	0.1		
FB Leakage Current	IFB	V _{FB} = 1.3V, T _A = +85°C		0.01		μA	
ON, SKIP Input High Voltage	VIH	2.5V < V _{IN} < 5.5V	1.6			V	
ON, SKIP Input Low Voltage	VIL	$2.5V < V_{IN} < 5.5V$			0.45	V	
ON Input Leakage Current	lu u	$2.5V < V_{IN} < 5.5V, T_A = +25^{\circ}C$		0.001	1		
ON Input Leakage Current	lihl	$T_A = +85^{\circ}C$		0.01		μA	
SKIP Input Leakage Current	ISKIPH	$V_{\overline{\text{SKIP}}} = 3.6V$		3	12		
SKIP Input Leakage Current	ISKIPL	$V_{\overline{SKIP}} = 0V$	-2	-0.2		μA	
Peak Current Limit	ILIMP	LX1 PMOS	1700	2000	2300	mA	
Fault Latch-Off Delay				100		ms	
		Each MOSFET, $T_A = +25^{\circ}C$		0.05	0.1		
MOSFET On-Resistance	R _{ON}	Each MOSFET, V_{IN} = 2.5V to 5.5V, T _A = -40°C to +85°C			0.2	Ω	
Rectifier-Off Current Threshold	ILX10FF	SKIP = GND		125		mA	
Idle-Mode Current Threshold	L	$\overline{\text{SKIP}}$ = GND, load decreasing		100			
(Note 4)	ISKIP	Load increasing		300		mA	
LX1, LX2 Leakage Current	I _{LXLKG}	$ V_{\text{IN}} = V_{\text{OUT}} = 5.5 \text{V}, \ V_{\text{LX1}} = 0 \text{V to } \text{V}_{\text{IN}}, \\ V_{\text{LX2}} = 0 \text{V to } \text{V}_{\text{OUT}}, \ T_{\text{A}} = +25^{\circ}\text{C} $		0.01	1	μA	
		$T_A = +85^{\circ}C$		0.2			
Out Reverse Current	I _{LXLKGR}	$\label{eq:VIN} \begin{split} V_{IN} = V_{LX1} = V_{LX2} = 0V, V_{OUT} = 5.5V, \\ measure \ I \ (LX2), T_A = +25^{\circ}C \end{split}$		0.01	1	μA	
		$T_A = +85^{\circ}C$		0.5			
Minimum T _{ON}	TONMIN			25		%	
OSC Frequency	Foscpwm		850	1000	1150	kHz	
Thermal Shutdown		15°C hysteresis		+165		°C	

Note 2: The device is production tested at $T_A = +25^{\circ}$ C. Specifications over the operating temperature range are guaranteed by design and characterization.

Note 3: Limits are guaranteed by design and not production tested.

Note 4: The idle-mode current threshold is the transition point between fixed-frequency PWM operation and idle-mode operation. The specification is given in terms of output load current for an inductor value of 3.3µH. For the step-up mode, the idle-mode transition varies with input to the output-voltage ratios.

Typical Operating Characteristics

 $(V_{IN} = 3.6V, \overline{SKIP} = GND, T_A = +25^{\circ}C, Figure 4, unless otherwise noted.)$

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EFFICIENCY vs. LOAD CURRENT SKIP-MODE EFFICIENCY EFFICIENCY vs. LOAD CURRENT SKIP AND FPWM MODES vs. INPUT VOLTAGE **FPWM MODE (FIGURE 3)** 100 100 100 90 90 95 80 80 90 300mA 70 70 (%) 85 % EFFICIENCY (%) 60 60 100mA EFFICIENCY EFFICIENCY 80 50 50 500mA VOUT = 3.3V $V_{OUT} = 2.8V$ 40 40 $V_{IN} = 2.7V$ 75 $V_{IN} = 2.7V$ 3.0V 3.0V 30 30 3.3V 70 3 3V 20 20 $V_{OUT} = 3.3V$ 3.6V 3.6V 4.2V 65 LOAD CURRENT = 100mA 10 10 4.2V 300mA, 500mA 5.0V 5.0V 0 60 0 2.0 2.5 3.0 3.5 4.0 4.5 5.0 5.5 6.0 0.1 1 10 100 1000 0.1 1 10 100 1000 LOAD CURRENT (mA) INPUT VOLTAGE (V) LOAD CURRENT (mA) **OUTPUT VOLTAGE (3.3V INTERNAL FB) EFFICIENCY vs. LOAD CURRENT OUTPUT VOLTAGE (2.8V EXTERNAL FB) FPWM MODE (FIGURE 3)** vs. LOAD CURRENT vs. LOAD CURRENT (FIGURE 3) 2.0 100 2.0 90 1.5 1.5 80 1.0 1.0 70 0.5 EFFICIENCY (%) DEVIATION (%) (%) 0.5 60 **DEVIATION** 0 50 0 $V_{OUT} = 3.45V$ 40 $V_{IN} = 2.7V$ -0.5 -0.5 3 0V 30 -1.0 -1.0 3.3V 20 3 6V -1.5 $V_{OUT} = 3.3$ -1.5 $V_{OUT} = 2.8V$ 4 2V 10 $T_A = +25^{\circ}C, T_A =$ -40°C. T∆ = +85°C $T_A = +25^{\circ}C$, $T_A = -40^{\circ}C$, $T_A = +85^{\circ}C$ 5.0\ -2.0 0 -2.0 0.1 10 1 100 1000 0.1 10 100 1000 0.1 10 100 1000 1 LOAD CURRENT (mA) LOAD CURRENT (mA) LOAD CURRENT (mA) SUPPLY CURRENT vs. INPUT VOLTAGE **OUTPUT VOLTAGE vs. INPUT VOLTAGE OUTPUT VOLTAGE vs. INPUT VOLTAGE** WITH INTERNAL FB RESISTORS WITH EXTERNAL FB RESISTORS WITH NO LOAD 100 2.82 3.33 2.81 FPWM MODE 3.32 10 () 3.31 3.30 3.30 3.29 () 2.80 2.79 2.79 2.78 2.78 SUPPLY CURRENT (mA) 1 2.77 0.1 ■ NO LOAD V_{OUT} = 3.3V 3.28 LOAD: 500mA, V_{OUT} = 3.3V 2.76 LOAD: 500mA, V_{OUT} = 2.8V $T_A = +25^{\circ}C, T_A = -40^{\circ}C, T_A = +85^{\circ}C$ T_A = +25°C, T_A = -40°C, T_A = +85°C (FIGURE 3) 3.27 2.75 0.01 2.5 3.0 3.5 4.0 4.5 20 50 55 60 3.0 3.5 4.0 4.5 5.0 5.5 6.0 3.0 3.5 4.0 4.5 5.0 5.5 6.0 INPUT VOLTAGE (V) INPUT VOLTAGE (V) INPUT VOLTAGE (V)

Typical Operating Characteristics (continued)

 $(V_{IN} = 3.6V, \overline{SKIP} = GND, T_A = +25^{\circ}C, Figure 4, unless otherwise noted.)$









SWITCHING WAVEFORMS $V_{IN} = 3.6V$, LOAD = 500mA, $V_{OUT} = 3.3V$





N = 3V, LOAD = 20mA Vout = 3.308V





Typical Operating Characteristics (continued)

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Typical Operating Characteristics (continued)

 $(V_{IN} = 3.6V, \overline{SKIP} = GND, T_A = +25^{\circ}C, Figure 4, unless otherwise noted.)$

















Pin Description

PIN	NAME	FUNCTION
1, 2	LX1	Inductor Connection 1. Connect the inductor between LX1 and LX2. Both LX1 pins must be connected together externally. LX1 is internally connected to GND during shutdown.
3, 4	LX2	Inductor Connection 2. Connect the inductor between LX1 and LX2. Both LX2 pins must be connected together externally. LX2 is internally connected to GND during shutdown.
5	ON	Enable Input. Connect ON to the input or drive high to enable the IC. Drive ON low to disable the IC.
6	SKIP	Mode Select Input. Connect SKIP to GND to enable skip mode. This mode provides the best overall efficiency curve. Connect SKIP to IN to enable forced-PWM mode. This mode provides the lowest noise, but reduces light-load efficiency compared to skip mode.
7	FB	Feedback Input. Connect to ground to set the fixed 3.3V output. Connect FB to the center tap of an external resistor-divider from the output to GND to set the output voltage to a different value. V _{FB} regulates to 1.25V.
8	REF	Reference Output. Bypass REF to GND with a 0.1μ F ceramic capacitor. V _{REF} is 1.25V and is internally pulled to GND during shutdown.
9, 10	OUT	Power Output. Bypass OUT to GND with two 22µF ceramic capacitors. Both OUT pins must be connected together externally.
11, 12	GND	Ground. Connect the exposed pad and GND directly under the IC.
13, 14	IN	Power-Supply Input. Bypass IN to GND with two 22µF ceramic capacitors. Connect IN to a 2.5V to 5.5V supply. Both IN pins must be connected together externally.
	EP	Exposed Pad. Connect to GND directly under the IC. Connect to a large ground plane for increased thermal performance.

Detailed Description

The MAX8625A step-up/down architecture employs a true H-bridge topology that combines a boost converter and a buck converter topology using a single inductor and output capacitor (Figure 1). The MAX8625A utilizes a pulse-width modulated (PWM), current-mode control scheme and operates at a 1MHz fixed frequency to minimize external component size. A proprietary H-bridge design eliminates mode changes when transitioning from buck to boost operation. This control scheme provides very low output ripple using a much smaller inductor than a conventional H-bridge, while avoiding glitches that are commonly seen during mode transitions with competing devices.

The MAX8625A switches at an internally set frequency of 1MHz, allowing for tiny external components. Internal compensation further reduces the external component count in cost- and space-sensitive applications. The MAX8625A is optimized for use in HDDs, DSCs, and other devices requiring low-quiescent current for optimal light-load efficiency and maximum battery life.

Control Scheme

The MAX8625A basic noninverting step-up/down converter operates with four internal switches. The control logic determines which two internal MOSFETs operate to maintain the regulated output voltage. Unlike a traditional H-bridge, the MAX8625A utilizes smaller peakinductor currents, thus improving efficiency and lowering input/output ripple.

The MAX8625A uses three operating phases during each switching cycle. In phase 1 (fast-charge), the inductor current ramps up with a di/dt of V_{IN}/L. In phase 2 (slow charge/discharge), the current either ramps up or down depending on the difference between the input voltage and the output voltage (V_{IN} - V_{OUT})/L. In phase 3 (discharge), the inductor current discharges at a rate of V_{OUT}/L through MOSFETs P2 and N1 (see Figure 1). An additional fourth phase (phase 4: hold) is entered when the inductor current falls to zero during phase 3. This fourth phase is only used during skip operation.

The state machine (Figure 2) decides which phase to use and when to switch phases. The converter goes through the first three phases in the same order at all



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Figure 1. Simplified Block Diagram

times. This reduces the ripple and removes any mode transitions from boost-only or buck-only to hybrid modes as seen in competing H-bridge converters.

The time spent in each phase is set by a PWM controller, using timers and/or peak-current regulation on a cycle-by-cycle basis. The heart of the PWM control block is a comparator that compares the output voltage-error feedback signal and the sum of the currentsense and slope compensation signals. The currentmode control logic regulates the inductor current as a function of the output error voltage signal. The currentsense signal is monitored across the MOSFETs (P1, N1, and N2). A fixed time delay of approximately 30ns occurs between turning the P1 and N2 MOSFETs off, and turning the N1 and P2 MOSFETs on. This dead time prevents efficiency loss by preventing "shootthrough" current.

Step-Down Operation (VIN > VOUT)

During medium and heavy loads and $V_{IN} > V_{OUT}$, MOSFETS P1 and N2 turn on to begin phase 1 at the clock edge and ramp up the inductor current. The duration of phase 1 is set by an internal timer. During phase 2, N2 turns off, and P2 turns on to further ramp up inductor current and also transfer charge to the output. This slow charge phase is terminated on a clock edge and P1 is turned off. The converter now enters the fast discharge phase (phase 3). In phase 3, N1 turns on and the inductor current ramps down to the valley current-regulation point set by the error signal. At the end of phase 3, both P2 and N1 turn off and another phase 1 is initiated and the cycle repeats.

With SKIP asserted low, during light loads when inductor current falls to zero in phase 3, the converter switches to phase 4 to reduce power consumption and avoid



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Figure 2. State Diagram

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shuttling current in and out of the output capacitor. If SKIP is asserted high for forced-PWM mode, phase 4 is not entered and current shuttling is allowed (and is necessary to maintain the PWM operation frequency when no load is present).

Step-Up Operation (VIN < VOUT)

During medium and heavy loads when $V_{IN} < V_{OUT}$, MOSFETs P1 and N2 turn on at the clock edge to ramp up the inductor current. Phase 1 terminates when the inductor current reaches the peak target current set by the PWM comparator and N2 turns off. This is followed by a slow-discharge phase (phase 2) instead of a charge phase (since V_{IN} is less than V_{OUT}) when P2 turns on. The slow-discharge phase terminates on a clock edge. The converter now enters the fast-discharge phase (phase 3). During phase 3, P1 turns off and N1 turns on. At the end of the minimum time, both P2 and N1 turn off and the cycle repeats.

If SKIP is asserted low, during light loads when inductor current falls to zero in phase 3, the converter switches to phase 4 (hold) to reduce power consumption and avoid shuttling current in and out of the output. If SKIP is high to assert forced-PWM mode, the converter never enters phase 4 and allows negative inductor current.

Step-Up/Down Transition-Zone Operation (VIN = VOUT)

When $V_{IN} = V_{OUT}$, the converter still goes through the three phases for moderate to heavy loads. However, the maximum time is now spent in phase 2 where inductor current di/dt is almost zero, since it is proportional to ($V_{IN} - V_{OUT}$). This eliminates transition glitches



or oscillation between the boost and buck modes as seen in other step-up/down converters. See the switching waveforms for each of the three modes and transition waveforms in the *Typical Operating Characteristics* section.

Forced-PWM Mode

Drive SKIP high to operate the MAX8625A in forced-PWM mode. In this mode, the IC operates at a constant 1MHz switching frequency with no pulse skipping. This scheme is desirable in noise-sensitive applications because the output ripple is minimized and has a predictable noise spectrum. Forced PWM consumes higher supply current at light loads due to constant switching.

Skip Mode

Drive SKIP low to operate the MAX8625A in skip mode to improve light-load efficiency. In skip mode, the IC switches only as necessary to maintain the output at light loads, but still operates with fixed-frequency PWM at medium and heavy loads. This maximizes light-load efficiency and reduces the input quiescent current to 37µA (typ).

Do not dynamically transition between skip and FPWM. The MAX8625A is not designed for dynamic transitions between FPWM and skip modes. Spikes of negative inductor current are possible when making these types of dynamic transitions. The magnitude of the spike depends on the load and output capacitance. The MAX8625A has no protection against these types of negative current spikes.

Load Regulation and Transient Response

During a load transient, the output voltage instantly changes due to the ESR of the output capacitors by an amount equal to their ESR times the change in load current ($\Delta V_{OUT} = R_{ESR} \times \Delta I_{LOAD}$). The output voltage then deviates further based on the speed at which the loop compensates for the load step. Increasing the output capacitance reduces the output-voltage droop. See the *Capacitor Selection* section. The typical application circuit limits the output transient droop to less than 3%. See the *Typical Operating Characteristics* section.

Soft-Start

Soft-start prevents input inrush current during startup. Internal soft-start circuitry ramps the peak inductor current with an internal DAC in 8ms. Once the output reaches regulation, the current limit immediately jumps to the maximum threshold. This allows full load capability as soon as regulation is reached, even if it occurs before the 8ms soft-start time is complete.

When using the MAX8625A at low input voltages (close to UVLO and < 3V), it is recommended that the ON pin should not be tied to the BATT or supply voltage node directly. The ON pin should be held low for > 1ms after power to the MAX8625A is applied before it is driven high for normal operation.

Shutdown

Drive ON low to place the MAX8625A in shutdown mode and reduce supply current to less than 1μ A. During shutdown, OUT is disconnected from IN, and LX1 and LX2 are connected to GND. Drive ON high for normal operation.

Fault and Thermal Shutdown

The MAX8625A contains current-limit and thermal shutdown circuitry to protect the IC from fault conditions. When the inductor current exceeds the current limit (2A for the MAX8625A), the converter immediately enters phase 3 and an internal 100ms timer starts. The converter continues to commutate through the three phases, spending most of its time in phase 1 and phase 3. If the overcurrent event continues and the output is out of regulation for the duration of the 100ms timer, the IC enters shutdown mode and the output latches off. ON must then be toggled to clear the fault. If the overload is removed before the 100ms timer expires, the timer is cleared and the converter resumes normal operation.

The thermal-shutdown circuitry disables the IC switching if the die temperature exceeds +165°C. The IC begins soft-start once the die temperature cools by 15°C.

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Applications Information

Selecting the Output Voltage

The MAX8625A output is nominally fixed at 3.3V. Connect FB to GND to select the internally fixed-output voltage. For an adjustable output voltage, connect FB to the center tap of an external resistor-divider connected from the output to GND (R1 and R2 in Figure 3). Select 100k Ω for R2 and calculate R1 using the following equation:

$$\text{R1} = 100 \text{k} \Omega \times \left(\frac{\text{V}_{\text{OUT}}}{\text{V}_{\text{FB}}} - 1 \right)$$

where $V_{FB} = 1.25V$ and V_{OUT} is the desired output regulation voltage. V_{OUT} must be between 1.25V and 4V. Note that the minimum output voltage is limited by the minimum duty cycle. V_{OUT} cannot be below 1.25V.

Calculating Maximum Output Current

The maximum output current provided by the MAX8625A circuit depends on the inductor value, switching frequency, efficiency, and input/output voltage.

See the *Typical Operating Characteristics* section for the Maximum Load Current vs. Input Voltage graph.

Capacitor Selection

The input and output ripple currents are both discontinuous in this topology. Therefore, select at least two 22μ F ceramic capacitors at the input. Select two 22μ F ceramic output capacitors. For best stability over a wide temperature range, use X5R or better dielectric.

Inductor Selection

The recommended inductance range for the MAX8625A is 3.3μ H to 4.7μ H. Larger values of L give a smaller ripple, while smaller L values provide a better transient response. This is because, for boost and step-up/down topologies, the crossover frequency is inversely proportional to the value of L for a given load and input voltage. The MAX8625A is internally compensated, and therefore, the choice of power components for stable operation is bounded. A 3.3μ H inductor with 2A rating is recommended for the 3.3V fixed output with 0.8A load.

PCB Layout and Routing

Good PCB layout is important to achieve optimal performance from the MAX8625A. Poor design can cause excessive conducted and/or radiated noise. Conductors carrying discontinuous currents and any high-current path should be made as short and wide as possible. Keep the feedback network (R1 and R2) very close to the IC, preferably within 0.2 inches of the FB and GND pins. Nodes with high dv/dt (switching nodes) should be kept as small as possible and routed away from FB. Connect the input and output capacitors as close as possible to the IC. Refer to the MAX8625A evaluation kit for a PCB layout example.



Figure 3. Typical Application Circuit (Adjustable Output)



Figure 4. Typical Application Circuit (Fixed 3.3V Output)

Chip Information

PROCESS: BICMOS

Package Information

For the latest package outline information and land patterns, go to **www.maxim-ic.com/packages**.

PACKAGE TYPE	PACKAGE CODE	DOCUMENT NO.
14 TDFN-EP	T1433-2	<u>21-0137</u>

Package Information (continued)

For the latest package outline information and land patterns, go to www.maxim-ic.com/packages.



Package Information (continued)

For the latest package outline information and land patterns, go to www.maxim-ic.com/packages.

COMMON	I DIMEN	SIONS		PACKAGE V	ARIAT	IONS					
SYMBOL	MIN.	MAX.		PKG. CODE	N	D2	E2	е	JEDEC SPEC	b	[(N/2)-1] x e
А	0.70	0.80		T633-2	6	1.50±0.10	2.30±0.10	0.95 BSC	MO229 / WEEA	0.40±0.05	1.90 REF
D	2.90	3.10		T833-2	8	1.50±0.10	2.30±0.10	0.65 BSC	MO229 / WEEC	0.30±0.05	1.95 REF
E	2.90	3.10		T833-3	8	1.50±0.10	2.30±0.10	0.65 BSC	MO229 / WEEC	0.30±0.05	1.95 REF
A1	0.00	0.05		T1033-1	10	1.50±0.10	2.30±0.10	0.50 BSC	MO229 / WEED-3	0.25±0.05	2.00 REF
L	0.20	0.40		T1033MK-1	10	1.50±0.10	2.30±0.10	0.50 BSC	MO229 / WEED-3	0.25±0.05	2.00 REF
k	0.25	MIN.		T1033-2	10	1.50±0.10	2.30±0.10	0.50 BSC	MO229 / WEED-3	0.25±0.05	2.00 REF
A2	0.20	REF.		T1433-1	14	1.70±0.10	2.30±0.10	0.40 BSC		0.20±0.05	2.40 REF
				T1433-2	14	1.70±0.10	2.30±0.10	0.40 BSC		0.20±0.05	2.40 REF
				T1433-3F	14	1.70±0.10	2.30±0.10	0.40 BSC		0.20±0.05	2.40 REF
NOTES					I	<u> </u>		0.10 000	I	0.2020.00	2.40 KEF
 COPL WARP PACK DRAW "N" IS NUMB 	ANARITY AGE SH AGE LEI ING COI S THE T ER OF	SHALL ALL NO NGTH/P/ NFORMS TOTAL N LEADS	NOT EX EXCEE ACKAGE TO JED UMBER SHOWN	A. ANGLES IN CEED 0.08 m D 0.10 mm. WIDTH ARE CC EC M0229, E OF LEADS. ARE FOR REF	m. DNSID XCEP	REES. ERED AS S T DIMENSIO CE ONLY.	PECIAL CHA NS "D2" AN	RACTERISTI	C(S). ND T1433-1 & T ¹		2.40 KEF
1. ALL D 2. COPL 3. WARP 4. PACK 5. DRAW 6. "N" IS 7. NUMB	ANARITY AGE SH AGE LEI ING COI S THE 1 ER OF ING IS	SHALL NGTH/P/ NFORMS TOTAL N LEADS FOR PA	NOT EX EXCEE ACKAGE TO JED UMBER SHOWN CKAGE C	n. ANGLES IN CEED 0.08 m D 0.10 mm. WIDTH ARE CC EC M0229, E DF LEADS.	m. DNSID XCEP EREN EFER	REES. ERED AS S T DIMENSIO CE ONLY. ENCE ONLY	PECIAL CHA NS "D2" AN	NRACTERISTI ND "E2", AN			2.40 KEF

Revision History

REVISION NUMBER	REVISION DATE	DESCRIPTION	PAGES CHANGED
0	3/08	Initial release	—
1	5/08	Added PCB Layout and Routing section	12
2	10/08	Updated Electrical Characteristics, Skip Mode and Soft-Start sections	2, 11
3	12/08	Corrected P1 and P2 symbols in Figure 1	9

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