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 $R_1(R_2)$  is a resistance that decides input current, by which the IC input is decided to be about 1mA. For example, when full scale is 100W, if  $R_L = 8\Omega$  load,  $R_1(R_2)$  is expressed as follows:

$$P_{OUT} = \frac{V^2 (V.rms)}{R_L(8\Omega)} \qquad V = \sqrt{P \times R_L} = \sqrt{100 \times 8} = 28.28 V rms$$
$$V_{IN} = 1mA \times R_1(R_2) = 28.28 V$$
$$R_1(R_2) = 28.28 k\Omega \qquad 27 k\Omega \text{ is used for } R_1(R_2)$$

2. DECISION OF R5(R6)

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 $R_5(R_6)$  is a shunt resistance that decides angle of a meter, by which the meter is adjusted so as to become full scale when the IC input is 1mA.



For example, when 1mA enters the input, the output is about. 4mA. (Refer to  $I_{\rm IN}$  -  $I_{\rm OUT}$ 

characteristics shown in the attached sheet.) Therefore, if a meter of lmA in meter sensitivity and  $680\,\Omega$  in internal impedance is used, the following equation is expressed:

$$R_5(R_6) = \frac{680}{3} = 226.7 \ddagger 220\Omega$$

Since  $R_5(R_6)$  has meter variations, the use of variable resistance enables right and left adjustments to be made more easily.



3. DECISION OF R3(R4)

 $R_3(R_4)$  is a resistance that decides supply current, by which pin 9 and pin 5 are fixed to GND (Pin 1) at  $\pm 8.5V$  respectively. Therefore, the value of  $R_3(R_4)$  should be decided so that the current flown into IC by supply voltage may become 10mA ~ 20mA.

For example, when  $R_3(R_4)$  is used at  $V_{CC}$ = 25V and  $V_{EE}$  =-25V, if it has 10% supply voltage variation, the following equation is obtained:

 $R_3(R_4) \geq \frac{25 \times 1.1 - 8.5V}{20 \text{mA}} k\Omega = 0.95 k\Omega$ 

If R3(R4) is  $1k\Omega$ , the supply current becomes 19mA.

In this case, if  $R_3(R_4)$  is  $1.2k\Omega$  by taking the power and variation into consideration, the supply current is expressed as follows:

$$I = \frac{25 - 8.5}{1.2k\Omega} = 13.8 \text{mA}$$

Since  $P = I^2R = 13.8^{2}mA \times 1.2k\Omega \doteq 230mW$ , the resistance of 1/4W type is sufficient. (Refer to  $I_{CC}$ -  $I_{OUT}$  shown in the data sheet.)

## 4. DECISION OF $C_1(C_2)$

 $C_1(C_2)$  is a capacity that decides the recovery time of a meter. A capacitor to be used should be lower in variation; for example, it is recommended that mylar film capacitor be used. The capacitor is classified into two ranks according to recovery time variations.

The typical values are shown as follows: (The recovery time from  $OdB \rightarrow -40dB$  is about.  $2 \sim 4 \sec$ .)

Classification	C <sub>1</sub> (C <sub>2</sub> )
TA7318P-1	0.0068#F
TA7318P-2	0.022 <i>µ</i> F

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≈≈AUDIO LINEAR IC≈

(Refer to  $C_1(C_2)$ -TRECA shown in the data sheet.)

## DE 9097247 0017095 4 TOSHIBA, ELECTRONIC D2 9097247 TOSHIBA. ELECTRONIC 02E 17095 D T-77-21 TA7318P 5. PRECAUTIONS AT TURN OF METER SENSITIVITY When the signal scurce impedance $R_1(R_2)$ is remarkably changed, the variations R1(R2) in amplification at the time of small input to the meter are apt to generate; TC therefore, these variations must be 204 B $R_{1}(R_{2})$

In this case, however,  $r < R_1(R_2)$ .

attenuated without changing the

impedance.

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6. CONNECTION OF R1 AND R7 TO CIRCUIT WHICH RELAY IS USED FOR OUTPUT TERMINAL



The resistance  $(R_7)$  should be inserted between input and ground as shown in the above figure. This is because the resistance prevents the ocurrence of such a phenomenon as, as long as the relay is turned OFF, the input impedance of TA7318P becomes high to be liable to receive the surrounding noise.

It is recommended that  $R_1$  and  $R_7$  be arranged close to the IC as far as possible.

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