19-0440; Rev 2; 4/97

EVALUATION KIT AVAILABLE

# Single/Dual/Quad, 400MHz, Low-Power, Current Feedback Amplifiers

## \_General Description

The single MAX4112/MAX4113, dual MAX4117/ MAX4118, and quad MAX4119/MAX4120 current feedback amplifiers combine high-speed performance with low-power operation. The MAX4112/MAX4117/ MAX4119 are optimized for closed-loop gains of 2V/V or greater, while the MAX4113/MAX4118/MAX4120 are optimized for gains of 8V/V or greater.

The MAX4112/MAX4117/MAX4119 and the MAX4113/ MAX4118/MAX4120 require only 5mA of supply current per channel, and deliver 0.1dB gain flatness up to 115MHz and -3db bandwidths of 400MHz (A<sub>V</sub>  $\geq$  2V/V) and 300MHz (A<sub>V</sub>  $\geq$  8V/V), respectively. Their high slew rates of up to 1800V/µs provide exceptional full-power bandwidths up to 280MHz, making these amplifiers ideal for high-performance pulse and RGB video applications.

These high-speed op amps have a wide output voltage swing of  $\pm 3.5V$  into  $100\Omega$  and a high current-drive capability of 80mA.

### Applications

Broadcast and High-Definition TV Systems

- RGB Video
- Pulse/RF Amplifier
- Ultrasound/Medical Imaging
- Active Filters
- High-Speed ADC Buffers
- Professional Cameras
- High-Definition Surveillance

#### \_Features

- 400MHz -3dB Bandwidth (MAX4112/MAX4117) 270MHz -3dB Bandwidth (MAX4113/MAX4119) 300MHz -3dB Bandwidth (MAX4118/MAX4120)
- 0.1dB Gain Flatness to 115MHz
- 1200V/µs Slew Rate (MAX4112/MAX4117/MAX4119)
  1800V/µs Slew Rate (MAX4113/MAX4118/MAX4120)
- 280MHz Full-Power Bandwidth (Vo = 2Vp-p, MAX4112/MAX4117) 240MHz Full-Power Bandwidth (Vo = 2Vp-p, MAX4113/MAX4118/MAX4120)
- + High Output Drive: 80mA
- + Low Power: 5mA Supply Current per Channel

## Ordering Information

PART	TEMP. RANGE	PIN-PACKAGE
MAX4112ESA	-40°C to +85°C	8 SO
MAX4112EUA	-40°C to +85°C	8 µMAX*
MAX4113ESA	-40°C to +85°C	8 SO
MAX4117ESA	-40°C to +85°C	8 SO
MAX4118ESA	-40°C to +85°C	8 SO

**Ordering Information continued at end of data sheet.** \*Contact factory for µMAX package availability.

## \_Pin Configurations



### M/X/W

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## **ABSOLUTE MAXIMUM RATINGS**

Power-Supply Voltage (V <sub>CC</sub> to V <sub>EE</sub> )
Short-Circuit Duration (VOUT to GND)
VIN < 1.5VContinuous
V <sub>IN</sub> > 1.5VOsec
Continuous Power Dissipation ( $T_A = +70^{\circ}C$ )
8-Pin SO (derate 5.88mW/°C above +70°C)471mW

8-Pin µMAX (derate 4.10mW/°C above +70°C)
14-Pin SO (derate 8.33mW/°C above +70°C)667mW
16-Pin QSOP (derate 9.52mW/°C above +70°C)762mW
Operating Temperature Range
MAX41E40°C to +85°C
Storage Temperature Range65°C to +160°C
Lead Temperature (soldering, 10sec)+300°C

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## **ELECTRICAL CHARACTERISTICS**

 $(V_{CC} = +5V, V_{EE} = -5V, T_A = T_{MIN}$  to  $T_{MAX}$ , unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ .) (Note 1)

PARAMETER	SYMBOL	CON	MIN	TYP	MAX	UNITS	
<b>DC SPECIFICATIONS</b> ( $R_L = \infty$ ,	unless other	wise noted)					
Input Offset Voltage	Vos	V <sub>OUT</sub> = 0V			1	8	mV
Input Offset Voltage Drift	TCVOS	V <sub>OUT</sub> = 0V			10		µV/°C
Positive Input Bias Current	I <sub>B+</sub>	$V_{OUT} = 0V, V_{IN} = -V_{OUT}$	DS		3.5	20	μA
Negative Input Bias Current	IB-	Vout = 0V, VIN = -Vo	DS		3.5	20	μA
Input Resistance		IN+			500		kΩ
Input Resistance		IN-	IN-		30		Ω
Input Voltage Noise	en	f = 10kHz			2.2		nV/√Hz
Integrated Voltage Noise	EnRMS	f = 1MHz to 100MHz			27		μV <sub>RMS</sub>
		6 40144	MAX4112/MAX4117/ MAX4119		13		– pA/√Hz
Positive Input Current Noise	in+	f = 10kHz	MAX4113/MAX4118/ MAX4120		9		
Negative Input Current Noise	i <sub>n-</sub>	f = 10kHz			14		pA/√Hz
Common-Mode Input Voltage	Vcm			-2.5		2.5	V
Common-Mode Rejection	CMR	$V_{CM} = \pm 2.5 V$	$V_{CM} = \pm 2.5 V$		50		dB
Power-Supply Rejection	PSR	$V_{S} = \pm 4.5 V \text{ to } \pm 5.5 V$		60	80		dB
Open-Loop Transimpedance	ZOL	$V_{OUT} = \pm 2.0V, V_{CM} =$	= 0V, $R_L$ = 100 $\Omega$	250	500		kΩ
Quiescent Supply Current per Amplifier	I <sub>SY</sub>	$V_{IN} = OV$			5	6.5	mA
Output Voltage Swing	Vout	RL = ∞		±3.5	±3.8		V
Output voltage Swillig	V001	$R_L = 100\Omega$		±3.1	±3.5		
Output Current Drive	IOUT	$R_L = 30\Omega$ , $T_A = 0^{\circ}C$ to $+85^{\circ}C$		65	80		mA
AC SPECIFICATIONS ( $R_L = 10$	$0\Omega$ , unless of	therwise noted)					
			MAX4112/MAX4117		400		
Small Signal -3dB Bandwidth	BWSS	$V_{OUT} \le 0.1 V_{RMS}$	MAX4113/MAX4119		270		MHz
-			MAX4118/MAX4120		300		

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#### **ELECTRICAL CHARACTERISTICS (continued)**

 $(V_{CC} = +5V, V_{EE} = -5V, T_A = T_{MIN}$  to  $T_{MAX}$ , unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ .) (Note 1)

PARAMETER	SYMBOL	COND	ITIONS	MIN TYP MAX	
AC SPECIFICATIONS (RL = 100	$\Omega$ , unless o				
	DW	MAX4112/MAX4117/W	100		
0.1dB Gain Flatness	BW <sub>0.1dB</sub>	MAX4113/MAX4118/MAX4120, A <sub>VCL</sub> = +8		115	— MHz
			MAX4112/MAX4117	280	
Lorge Cignel 2dD Depdwidth			MAX4119	145	MHz
Large-Signal -3dB Bandwidth	BWLS	V <sub>OUT</sub> = 2Vp-p	MAX4113/MAX4118/ MAX4120	240	- WHZ
Slew Rate	60		MAX4112/MAX4117/ MAX4119	1200	)//
	SR	$-2V \le V_{OUT} \le 2V$	MAX4113/MAX4118/ MAX4120	1800	— V/µs
		to 0.1%, -1V ≤ V <sub>OUT</sub> ≤ 1V	MAX4112/MAX4117/ MAX4119	15	
			MAX4113/MAX4118/ MAX4120	10	
Settling Time	ts	to 0.01%, -1V ≤ V <sub>OUT</sub> ≤ 1V	MAX4112/MAX4117/ MAX4119	35	— ns
			MAX4113/MAX4118/ MAX4120	25	
Rise/Fall Times	+_ +_	10% to 90%, -2V ≤ V <sub>O</sub>	10% to 90%, $-2V \le V_{OUT} \le 2V$ 10% to 90%, $-50mV \le V_{OUT} \le 50mV$		
Rise/Fail Times	t <sub>R</sub> , t <sub>F</sub>	10% to 90%, -50mV ≤			— ns
Differential Gain	DG	f = 3.58MHz,	MAX4112/MAX4117/ MAX4119, A <sub>VCL</sub> = +2	0.02	%
Direfential Gain	DG	$R_L = 150\Omega$	MAX4113/MAX4118/ MAX4120, A <sub>VCL</sub> = +8	0.02	70
Differential Phase	DP	f = 3.58MHz,	MAX4112/MAX4117/ MAX4119, A <sub>VCL</sub> = +2	0.03	- degrees
Direrential Phase	DP	$R_L = 150\Omega$	MAX4113/MAX4118/ MAX4120, A <sub>VCL</sub> = +8	0.04	- degrees
Input Capacitance	CIN	·		2	pF
Output Impedance	Zout	$f = 10MHz, A_{VCL} = +2$	$f = 10MHz, A_{VCL} = +2$		Ω
		$f_{\rm C} = 5 {\rm MHz},$	MAX4112/MAX4117/ MAX4119, A <sub>VCL</sub> = +2	-68	dBc
Spanous-rice Dynamic Kallye		V <sub>OUT</sub> = 2Vp-p	MAX4113/MAX4118/ MAX4120, A <sub>VCL</sub> = +8	-62	
Two-Tone Third-Order Intercept	IP3	MAX4112/MAX4117/MAX4119, $f_{C} = 10MHz$ , $f_{C1} = 10.1MHz$ , $A_{VCL} = +2$		36	dB
Crosstalk		All hostile, $V_{IN} = 1Vp-p$ , f = 10MHz		-75	dB

**Note 1:** The MAX4112/MAX4113/MAX4117–MAX4120 are designed to operate in a closed-loop configuration in which the IN- pin is driven by the OUT pin through an external feedback network. If an external voltage source is connected to IN-, current into or out of IN- must be limited to ±10mA, to prevent damage to the part.







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Typical Operating Characteristics (continued)



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_Pin Descriptions	_Pin	Descri	ptions
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P	N		
MAX4112 MAX4113 SO/µMAX	MAX4117 MAX4118 SO	NAME	FUNCTION
1, 5, 8	_	N.C.	No Connection. Not internally connected.
—	1	OUTA	Amplifier A Output
2	_	IN-	Inverting Input
—	2	INA-	Amplifier A Inverting Input
3		IN+	Noninverting Input
	3	INA+	Amplifier A Noninverting Input
4	4	Vee	Negative Power Supply. Connect to -5V.
	5	INB+	Amplifier B Noninverting Input
6		OUT	Amplifier Output
	6	INB-	Amplifier B Inverting Input
_	7	OUTB	Amplifier B Output
7	8	Vcc	Positive Power Supply. Connect to +5V.

## **Detailed Description**

The MAX4112/MAX4117/MAX4119 are optimized for closed-loop gains (AvcL) of 2V/V or greater, while the MAX4113/MAX4118/MAX4120 are optimized for closed-loop gains of 8V/V or greater. These low-power, high-speed, current feedback amplifiers operate from ±5V supplies. They are designed to drive video loads with low distortion characteristics. The MAX4112/MAX4117/MAX4119's differential gain and phase are 0.02% and 0.03°, respectively; the MAX4113/MAX4118/MAX4120 exhibit gain/phase error specifications of 0.02% and 0.04°, respectively. These characteristics, plus a wide 0.1dB gain flatness, make the MAX4112/MAX4113/MAX4117-MAX4120 ideal for use





P	PIN		
MAX4119	MAX4119/MAX4120		FUNCTION
SO	QSOP		
1	1	OUTA	Amplifier A Output
2	2	INA-	Amplifier A Inverting Input
3	3	INA+	Amplifier A Noninverting Input
4	4	V <sub>CC</sub>	Positive Power Supply. Connect to +5V.
5	5	INB+	Amplifier B Noninverting Input
6	6	INB-	Amplifier B Inverting Input
7	7	OUTB	Amplifier B Output
_	8, 9	N.C.	No Connection. Not internally connected.
8	10	OUTC	Amplifier C Output
9	11	INC-	Amplifier C Inverting Input
10	12	INC+	Amplifier C Noninverting Input
11	13	VEE	Negative Power Supply. Connect to -5V.
12	14	IND+	Amplifier D Noninverting Input
13	15	IND-	Amplifier D Inverting Input
14	16	OUTD	Amplifier D Output

in broadcast and graphics video systems. The combination of ultra-high speed and low power makes these parts suitable for use in general-purpose, high-speed applications, such as medical imaging, industrial instrumentation, and communications systems.

## Applications Information

#### Theory of Operation

Since these devices are current-feedback amplifiers, their open-loop transfer function is expressed as a transimpedance,  $\Delta V_{OUT}/\Delta I_{IN}$ , or ZoL. The frequency behavior of the open-loop transimpedance is similar to the open-loop gain of a voltage feedback amplifier. That is, it has a large DC value and decreases at approximately 6dB per octave.

Analyzing the follower with gain, as shown in Figure 1, yields the following transfer function:

$$\frac{V_{OUT}}{V_{IN}} = G \times \frac{Z_{OL}(S)}{Z_{OL}(S) + G \times (R_{IN} + R_F)}$$

where G = A<sub>VCL</sub> = 1 + (R<sub>F</sub> / R<sub>G</sub>), and R<sub>IN</sub> = 1 /g<sub>M</sub>  $\cong$  30 $\Omega$ .

At low gains, G x RIN << RF. Therefore, the closed-loop bandwidth is essentially independent of closed-loop gain. Similarly,  $Z_{OL} >> R_F$  at low frequencies, so that:

$$\frac{V_{OUT}}{V_{IN}} = G = 1 + (R_F / R_G)$$

#### Layout and Power-Supply Bypassing

The MAX4112/MAX4113/MAX4117–MAX4120 have an RF bandwidth and consequently require careful board layout, including the possible use of constant-impedance microstrip or stripline techniques.

To realize the full AC performance of these high-speed amplifiers, pay careful attention to power-supply bypassing and board layout. The PC board should have at least two layers: a signal and power layer on one side, and a large, low-impedance ground plane on the other side. The ground plane should be as free of voids as possible. With multilayer boards, locate the ground plane on a layer that incorporates no signal or power traces.

Regardless of whether a constant-impedance board is used, observe the following guidelines when designing the board. Wire-wrapped boards are much too inductive, and breadboards are much too capacitive; neither should be used. IC sockets increase parasitic capacitance and inductance, and should not be used. In general, surface-mount components give better highfrequency performance than through-hole components. They have shorter leads and lower parasitic reactances. Keep lines as short and as straight as possible. Do not make 90° turns; round all corners.

Observe high-frequency bypassing techniques to maintain the amplifier's accuracy. The bypass capacitors should include a 1000pF ceramic capacitor between each supply pin and the ground plane, located as close to the package as possible. Next, place a



Figure 2a. Inverting Gain Configuration



Figure 2b. Noninverting Gain Configuration

 $0.01\mu$ F to  $0.1\mu$ F ceramic capacitor in parallel with each 1000pF capacitor, and as close to them as possible. Then place a  $10\mu$ F to  $15\mu$ F low-ESR tantalum at the point of entry (to the PC board) of the power-supply pins. The power-supply trace should lead directly from the tantalum capacitor to the Vcc and VEE pins. To minimize parasitic inductance, keep PC traces short and use surface-mount components.

COMPONENT		Avcl = +2		A <sub>VCL</sub> = +8			
COMPONENT	MAX4112	MAX4117	MAX4119	MAX4113	MAX4118	MAX4120	
R <sub>F</sub> (Ω)	600	600	500	500	330	330	
R <sub>G</sub> (Ω)	600	600	500	69	47	47	
R <sub>O</sub> (Ω)	49.9	49.9	49.9	49.9	49.9	49.9	
R <sub>T</sub> (Ω)	49.9	49.9	49.9	49.9	49.9	49.9	
-3dB Small-Signal Bandwidth (MHz)	400	400	270	270	300	300	
0.1dB Gain Flatness (MHz)	100	100	100	115	115	115	
Large-Signal Bandwidth (MHz)	280	280	145	240	240	240	

Table 1. Recommended Component Values





Figure 3. Output Offset Voltage

**Choosing Feedback and Gain Resistors** 

The MAX4112/MAX4113/MAX4117–MAX4120 are current feedback amplifiers. Increasing feedback resistor values will decrease peaking. Use the input resistor (R<sub>G</sub>) to change the magnitude of the gain. Figure 2 shows the standard inverting and noninverting configurations. Notice that the gain of the noninverting circuit (Figure 2b) is 1 plus the magnitude of the inverting closed-loop gain (Table 1).

#### **DC and Noise Errors**

There are several major error sources to consider in any operational amplifier. These apply equally to the MAX4112/MAX4113/MAX4117–MAX4120. Offset-error terms are given by the equation below. Voltage and current-noise errors are root-square summed and therefore computed separately. In Figure 3, the total output offset voltage is determined by:

- a) The input offset voltage (Vos) times the closed-loop gain (1 + (R<sub>F</sub> / R<sub>G</sub>)).
- b) The positive input bias current ( $I_{B+}$ ) times the source resistor ( $R_S$ ) (usually 50 $\Omega$  or 75 $\Omega$ ), plus the negative input bias current ( $I_{B-}$ ) times the parallel combination of  $R_G$  and  $R_F$ . In current-mode feedback amplifiers, the input bias currents may flow into or out of the device. For this reason, there is no benefit to matching the resistance at both inputs.

The equation for total DC error is:

$$V_{OUT} = \left[ \left( I_{B+} \right) R_{S} + \left( I_{B-} \right) \left( R_{F} \parallel R_{G} \right) + V_{OS} \right] \left( 1 + \frac{R_{F}}{R_{G}} \right)$$

c) The total output-referred noise voltage is:

$$e_{n(OUT)} = \left(1 + \frac{R_F}{R_G}\right) \sqrt{\left[(i_{n+})R_S\right]^2 + \left[(i_{n-})R_F \mid \mid R_G\right]^2 + (e_n)^2}$$

The MAX4112/MAX4117/MAX4119 have a very low,  $2nV/\sqrt{Hz}$  noise voltage. The current noise at the positive input (i<sub>n+</sub>) is  $13pA/\sqrt{Hz}$ , and the current noise at the inverting input (i<sub>n-</sub>) is  $14pA/\sqrt{Hz}$ .

An example of the DC error calculations, using the MAX4112 typical data and the typical operating circuit where  $R_F = R_G = 600\Omega$  ( $R_F \parallel R_G = 300\Omega$ ) and  $R_S = 50\Omega$ , gives the following:

 $V_{OUT} = (3.5 \times 10^{-6} \times 50 + 3.5 \times 10^{-6} \times 300 + 10^{-3}) (1 + 1)$ 

 $V_{OUT} = 4.45 mV$ 

Calculating total output noise in a similar manner yields:

$$\begin{split} e_{n(OUT)} &= (1+1) \sqrt{\left(13 x 10^{-12} x 50\right)^2 + \left(14 x 10^{-12} x 300\right)^2 + \left(2 x 10^{-9}\right)^2} \\ e_{n(OUT)} &= 9.4 \text{nV} / \sqrt{\text{Hz}} \end{split}$$

With a 200MHz system bandwidth, this calculates to  $133\mu V_{RMS}$  (approximately 797 $\mu Vp$ -p, choosing the six-sigma value).

#### **Resistor Types**

Surface-mount resistors are the best choice for highfrequency circuits. They are of similar material to metalfilm resistors, but are deposited using a thick-film process in a flat, linear manner that minimizes inductance. Their small size and lack of leads also minimizes parasitic inductance and capacitance, yielding more predictable performance.

Metal-film resistors with leads are manufactured using a thin-film process where resistive material is deposited in a spiral layer around a ceramic rod. Although the materials used are noninductive, the spiral winding presents a small inductance (about 5nH) that may have an adverse effect on high-frequency circuits.

Carbon-composition resistors with leads are manufactured by pouring the resistor material into a mold. This process yields relatively low-inductance resistors that are very useful in high-frequency applications, although they tend to cost more and have more thermal noise than other types. The ability of carbon-composition resistors to self-heal after a large current overload makes them useful in high-power RF applications.

For general-purpose use, surface-mount metal-film resistors seem to have the best overall performance for low cost, low inductance, and low noise.

#### Video Line Driver

The MAX4112/MAX4113/MAX4117–MAX4120 are optimized (gain flatness) to drive coaxial transmission lines when the cable is terminated at both ends, as shown in Figure 4. Cable frequency response can cause variations in the flatness of the signal.

#### Driving Capacitive Loads

The MAX4112/MAX4113/MAX4117–MAX4120 are optimized for AC performance. They are not designed to drive highly capacitive loads. Reactive loads decrease phase margin and can produce excessive ringing and oscillation. Figure 5a shows a circuit that eliminates this problem. The small (usually 5 $\Omega$  to 22 $\Omega$ ) isolation resistor, Rs, placed before the reactive load prevents ringing and oscillation. At higher capacitive loads, AC performance is controlled by the interaction of the load capacitance and isolation resistor.



Figure 4. Video Line Driver



Figure 5a. Using an Isolation Resistor (Rs) for High Capacitive Loads

### \_Ordering Information (continued)

PART	TEMP. RANGE	PIN-PACKAGE
MAX4119ESD	-40°C to +85°C	14 SO
MAX4119EEE	-40°C to +85°C	16 QSOP*
MAX4120ESD	-40°C to +85°C	14 SO
MAX4120EEE	-40°C to +85°C	16 QSOP*

\* Contact factory for QSOP package availability.



Figure 5b. Frequency Response vs. Capacitive Load— No Isolation Resistor



Figure 5c. Frequency Response vs. Isolation Resistance (see Figure 5a for circuit)

### \_Chip Information

TRANSISTOR COUNT: 53 (MAX4112/MAX4113) 112 (MAX4117/MAX4118) 220 (MAX4119/MAX4120)

SUBSTRATE CONNECTED TO  $\mathsf{V}_{\mathsf{EE}}$ 

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