

## LM1577/LM2577 SIMPLE SWITCHER® Step-Up Voltage Regulator **General Description**

The LM1577/LM2577 are monolithic integrated circuits that provide all of the power and control functions for step-up (boost), flyback, and forward converter switching regulators. The device is available in three different output voltage versions: 12V, 15V, and adjustable.

Requiring a minimum number of external components, these regulators are cost effective, and simple to use. Listed in this data sheet are a family of standard inductors and flyback transformers designed to work with these switching regulators.

Included on the chip is a 3.0A NPN switch and its associated protection circuitry, consisting of current and thermal limiting, and undervoltage lockout. Other features include a 52 kHz fixed-frequency oscillator that requires no external components, a soft start mode to reduce in-rush current during start-up, and current mode control for improved rejection of input voltage and output load transients.

#### Features

- Requires few external components
- NPN output switches 3.0A, can stand off 65V
- Wide input voltage range: 3.5V to 40V
- Current-mode operation for improved transient response, line regulation, and current limit
- 52 kHz internal oscillator
- Soft-start function reduces in-rush current during start-up
- Output switch protected by current limit, under-voltage lockout, and thermal shutdown

**–** 5– V<sub>IN</sub>

■ 4- Switch

□ 3- Ground

□ 1- Comp

■ 2- Feedback

01146805

## Typical Applications

- Simple boost regulator
- Flyback and forward regulators
- Multiple-output regulator

## **Connection Diagrams**





Temperature	Package		Output Voltage		NSC	
Range	Туре	12V	15V	ADJ	Package	Package
					Drawing	
$40^{\circ}C \le T_A \le +125^{\circ}C$	24-Pin Surface Mount	LM2577M-12	LM2577M-15	LM2577M-ADJ	M24B	SO
	16-Pin Molded DIP	LM2577N-12	LM2577N-15	LM2577N-ADJ	N16A	N
	5-Lead Surface Mount	LM2577S-12	LM2577S-15	LM2577S-ADJ	TS5B	TO-263
	5-Straight Leads	LM2577T-12	LM2577T-15	LM2577T-ADJ	T05A	TO-220
	5-Bent Staggered	LM2577T-12	LM2577T-15	LM2577T-ADJ	T05D	TO-220
	Leads	Flow LB03	Flow LB03	Flow LB03		
$-55^{\circ}C \le T_{A} \le +150^{\circ}C$	4-Pin TO-3	LM1577K-12/883L	M1577K-15/883	LM1577K- ADJ/883	K04A	TO-3

## **Typical Application**



Note: Pin numbers shown are for TO-220 (T) package.

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## Absolute Maximum Ratings (Note 1)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

Supply Voltage	45V
Output Switch Voltage	65V
Output Switch Current (Note 2)	6.0A
Power Dissipation	Internally Limited
Storage Temperature Range	–65°C to +150°C
Lead Temperature	
(Soldering, 10 sec.)	260°C
Maximum Junction Temperature	150°C

## **Operating Ratings**

Supply Voltage	$3.5V \le V_{IN} \le 40V$
Output Switch Voltage	$0V \le V_{SWITCH} \le 60V$
Output Switch Current	$I_{SWITCH} \le 3.0A$
Junction Temperature Range	
LM1577	$-55^{\circ}C \le T_{J} \le +150^{\circ}C$
LM2577	$-40^{\circ}C \leq T_{J} \leq +125^{\circ}C$

### Electrical Characteristics—LM1577-12, LM2577-12

Specifications with standard type face are for  $T_J = 25$ °C, and those in **bold type face** apply over full **Operating Temperature Range**. Unless otherwise specified,  $V_{IN} = 5V$ , and  $I_{SWITCH} = 0$ .

				LM1577-12	LM2577-12	Units
Symbol	Parameter	Conditions	Typical	Limit	Limit	(Limits)
				(Notes 3, 4)	(Note 5)	
SYSTEM PA	RAMETERS Circuit of Figu	ure 1 (Note 6)				
V <sub>OUT</sub>	Output Voltage	$V_{IN} = 5V$ to 10V	12.0			V
		$I_{LOAD} = 100 \text{ mA to } 800 \text{ mA}$		11.60/ <b>11.40</b>	11.60/ <b>11.40</b>	V(min)
		(Note 3)		12.40/ <b>12.60</b>	12.40/ <b>12.60</b>	V(max)
ΔV <sub>OUT</sub>	Line Regulation	$V_{IN} = 3.5V$ to 10V	20			mV
ΔV <sub>IN</sub>		$I_{LOAD} = 300 \text{ mA}$		50/ <b>100</b>	50/ <b>100</b>	mV(max)
ΔV <sub>OUT</sub>	Load Regulation	V <sub>IN</sub> = 5V	20			mV
$\Delta_{LOAD}$		$I_{LOAD}$ = 100 mA to 800 mA		50/ <b>100</b>	50/ <b>100</b>	mV(max)
η	Efficiency	$V_{IN} = 5V, I_{LOAD} = 800 \text{ mA}$	80			%
DEVICE PAR	AMETERS	•				
I <sub>S</sub>	Input Supply Current	V <sub>FEEDBACK</sub> = 14V (Switch Off)	7.5			mA
				10.0/ <b>14.0</b>	10.0/ <b>14.0</b>	mA(max)
		I <sub>SWITCH</sub> = 2.0A	25			mA
		V <sub>COMP</sub> = 2.0V (Max Duty Cycle)		50/ <b>85</b>	50/ <b>85</b>	mA(max)
V <sub>UV</sub>	Input Supply	I <sub>SWITCH</sub> = 100 mA	2.90			V
	Undervoltage Lockout			2.70/ <b>2.65</b>	2.70/ <b>2.65</b>	V(min)
				3.10/ <b>3.15</b>	3.10/ <b>3.15</b>	V(max)
f <sub>o</sub>	Oscillator Frequency	Measured at Switch Pin	52			kHz
		I <sub>SWITCH</sub> = 100 mA		48/ <b>42</b>	48/ <b>42</b>	kHz(min)
				56/ <b>62</b>	56/ <b>62</b>	kHz(max)
V <sub>REF</sub>	Output Reference	Measured at Feedback Pin				V
	Voltage	$V_{IN} = 3.5V$ to 40V	12	11.76/ <b>11.64</b>	11.76/ <b>11.64</b>	V(min)
		$V_{COMP} = 1.0V$		12.24/ <b>12.36</b>	12.24/ <b>12.36</b>	V(max)
$\Delta V_{REF}$	Output Reference	$V_{IN} = 3.5V$ to 40V	7			mV
$\Delta V_{IN}$	Voltage Line Regulator					
R <sub>FB</sub>	Feedback Pin Input		9.7			kΩ
	Resistance					
G <sub>м</sub>	Error Amp	$I_{COMP} = -30 \ \mu A \text{ to } +30 \ \mu A$	370			µmho
	Transconductance	$V_{COMP} = 1.0V$		225/ <b>145</b>	225/ <b>145</b>	µmho(min
				515/ <b>615</b>	515/ <b>615</b>	µmho(max

**Electrical Characteristics**—LM1577-12, LM2577-12 (Continued) Specifications with standard type face are for  $T_J = 25$ °C, and those in **bold type face** apply over full **Operating Temperature Range**. Unless otherwise specified,  $V_{IN} = 5V$ , and  $I_{SWITCH} = 0$ .

				LM1577-12	LM2577-12	Units
Symbol	Parameter	Conditions	Typical	Limit	Limit	(Limits)
				(Notes 3, 4)	(Note 5)	
DEVICE PAR	AMETERS					
A <sub>VOL</sub>	Error Amp	$V_{COMP} = 1.1V$ to 1.9V	80			V/V
	Voltage Gain	$R_{COMP} = 1.0 M\Omega$		50/ <b>25</b>	50/ <b>25</b>	V/V(min)
		(Note 7)				
	Error Amplifier	Upper Limit	2.4			V
	Output Swing	$V_{\text{FEEDBACK}} = 10.0 \text{V}$		2.2/ <b>2.0</b>	2.2/ <b>2.0</b>	V(min)
		Lower Limit	0.3			V
		$V_{\text{FEEDBACK}} = 15.0V$		0.40/ <b>0.55</b>	0.40/ <b>0.55</b>	V(max)
	Error Amplifier	$V_{\text{FEEDBACK}} = 10.0V \text{ to } 15.0V$	±200			μA
	Output Current	$V_{COMP} = 1.0V$		±130/ <b>±90</b>	±130/ <b>±90</b>	µA(min)
				±300/ <b>±400</b>	±300/ <b>±400</b>	µA(max)
I <sub>ss</sub>	Soft Start Current	V <sub>FEEDBACK</sub> = 10.0V	5.0			μA
		$V_{COMP} = 0V$		2.5/ <b>1.5</b>	2.5/ <b>1.5</b>	µA(min)
				7.5/ <b>9.5</b>	7.5/ <b>9.5</b>	µA(max)
D	Maximum Duty Cycle	$V_{COMP} = 1.5V$	95			%
		I <sub>SWITCH</sub> = 100 mA		93/ <b>90</b>	93/ <b>90</b>	%(min)
ΔI <sub>SWITCH</sub>	Switch		12.5			A/V
$\Delta V_{COMP}$	Transconductance					
I <sub>L</sub>	Switch Leakage	V <sub>SWITCH</sub> = 65V	10			μA
	Current	$V_{\text{FEEDBACK}} = 15V$ (Switch Off)		300/ <b>600</b>	300/ <b>600</b>	µA(max)
V <sub>SAT</sub>	Switch Saturation	I <sub>SWITCH</sub> = 2.0A	0.5			V
	Voltage	V <sub>COMP</sub> = 2.0V (Max Duty Cycle)		0.7/ <b>0.9</b>	0.7/ <b>0.9</b>	V(max)
	NPN Switch		4.5			А
	Current Limit			3.7/ <b>3.0</b>	3.7/ <b>3.0</b>	A(min)
				5.3/ <b>6.0</b>	5.3/ <b>6.0</b>	A(max)

## Electrical Characteristics—LM1577-15, LM2577-15

Specifications with standard type face are for  $T_J = 25$ °C, and those in **bold type face** apply over full **Operating Temperature Range**. Unless otherwise specified,  $V_{IN} = 5V$ , and  $I_{SWITCH} = 0$ .

				LM1577-15	LM2577-15	Units
Symbol	Parameter	Conditions	Typical	Limit	Limit	(Limits)
				(Notes 3, 4)	(Note 5)	
SYSTEM PARA	METERS Circuit of Figure 2	2 (Note 6)				
V <sub>OUT</sub>	Output Voltage	$V_{IN} = 5V$ to 12V	15.0			V
		$I_{LOAD} = 100 \text{ mA to } 600 \text{ mA}$		14.50/ <b>14.25</b>	14.50/ <b>14.25</b>	V(min)
		(Note 3)		15.50/ <b>15.75</b>	15.50/ <b>15.75</b>	V(max)
ΔV <sub>OUT</sub>	Line Regulation	V <sub>IN</sub> = 3.5V to 12V	20			mV
$\Delta V_{IN}$		I <sub>LOAD</sub> = 300 mA		50/ <b>100</b>	50/ <b>100</b>	mV(max)
ΔV <sub>OUT</sub>	Load Regulation	$V_{IN} = 5V$	20			mV
$\Delta_{LOAD}$		$I_{LOAD}$ = 100 mA to 600 mA		50/ <b>100</b>	50/ <b>100</b>	mV(max)
η	Efficiency	$V_{IN} = 5V, I_{LOAD} = 600 \text{ mA}$	80			%

**Electrical Characteristics**—LM1577-15, LM2577-15 (Continued) Specifications with standard type face are for  $T_J = 25$ °C, and those in **bold type face** apply over full **Operating Temperature Range**. Unless otherwise specified,  $V_{IN} = 5V$ , and  $I_{SWITCH} = 0$ .

Symbol	Parameter	Conditions	Typical	LM1577-15 Limit (Notes 3, 4)	LM2577-15 Limit (Note 5)	Units (Limits)
DEVICE PARA	METERS			<u> </u>	, ,	
I <sub>S</sub>	Input Supply Current	V <sub>FEEDBACK</sub> = 18.0V (Switch Off)	7.5	10.0/ <b>14.0</b>	10.0/ <b>14.0</b>	mA mA(max)
		$I_{SWITCH} = 2.0A$ $V_{COMP} = 2.0V$ (Max Duty Cycle)	25	50/ <b>85</b>	50/ <b>85</b>	mA mA(max)
V <sub>UV</sub>	Input Supply Undervoltage	I <sub>SWITCH</sub> = 100 mA	2.90	2.70/ <b>2.65</b>	2.70/ <b>2.65</b>	V V(min)
	Lockout		_	3.10/ <b>3.15</b>	3.10/ <b>3.15</b>	V(max)
f <sub>o</sub>	Oscillator Frequency	Measured at Switch Pin I <sub>SWITCH</sub> = 100 mA	52	48/ <b>42</b> 56/ <b>62</b>	48/ <b>42</b> 56/ <b>62</b>	kHz kHz(min) kHz(max)
V <sub>REF</sub>	Output Reference	Measured at Feedback Pin				V
	Voltage	V <sub>IN</sub> = 3.5V to 40V V <sub>COMP</sub> = 1.0V	15	14.70/ <b>14.55</b> 15.30/ <b>15.45</b>	14.70/ <b>14.55</b> 15.30/ <b>15.45</b>	V(min) V(max)
$rac{\Delta V_{REF}}{\Delta V_{IN}}$	Output Reference Voltage Line Regulation	$V_{IN} = 3.5V$ to 40V	10			mV
R <sub>FB</sub>	Feedback Pin Input Voltage Line Regulator		12.2			kΩ
G <sub>м</sub>	Error Amp Transconductance	$I_{COMP} = -30 \ \mu A \ to +30 \ \mu A$ $V_{COMP} = 1.0V$	300	170/ <b>110</b> 420/ <b>500</b>	170/ <b>110</b> 420/ <b>500</b>	µmho µmho(min µmho(max
A <sub>VOL</sub>	Error Amp Voltage Gain	$V_{COMP} = 1.1V$ to 1.9V $R_{COMP} = 1.0 M\Omega$ (Note 7)	65	40/ <b>20</b>	40/ <b>20</b>	V/V V/V(min)
	Error Amplifier Output Swing	Upper Limit V <sub>FEEDBACK</sub> = 12.0V	2.4	2.2/ <b>2.0</b>	2.2/ <b>2.0</b>	V V(min)
		Lower Limit V <sub>FEEDBACK</sub> = 18.0V	0.3	0.4/ <b>0.55</b>	0.40/ <b>0.55</b>	V V(max)
	Error Amp Output Current	$V_{\text{FEEDBACK}} = 12.0V \text{ to } 18.0V$ $V_{\text{COMP}} = 1.0V$	±200	±130/ <b>±90</b> ±300/ <b>±400</b>	±130/ <b>±90</b> ±300/ <b>±400</b>	μΑ μA(min) μA(max)
I <sub>ss</sub>	Soft Start Current	$V_{\text{FEEDBACK}} = 12.0V$ $V_{\text{COMP}} = 0V$	5.0	2.5/ <b>1.5</b> 7.5/ <b>9.5</b>	2.5/ <b>1.5</b> 7.5/ <b>9.5</b>	μΑ μA(min) μA(max)
D	Maximum Duty Cycle	V <sub>COMP</sub> = 1.5V I <sub>SWITCH</sub> = 100 mA	95	93/ <b>90</b>	93/ <b>90</b>	%(min)
$\frac{\Delta I_{SWITCH}}{\Delta V_{COMP}}$	Switch Transconductance		12.5			A/V
I <sub>L</sub>	Switch Leakage Current	$V_{SWITCH} = 65V$ $V_{FEEDBACK} = 18.0V$ (Switch Off)	10	300/ <b>600</b>	300/ <b>600</b>	μΑ μA(max)
V <sub>SAT</sub>	Switch Saturation Voltage	$I_{SWITCH} = 2.0A$ $V_{COMP} = 2.0V$ (Max Duty Cycle)	0.5	0.7/ <b>0.9</b>	0.7/ <b>0.9</b>	V V(max)

•	······	$V_{IN} = 5V$ , and $I_{SWITCH} = 0$ .		1	г г	
				LM1577-15	LM2577-15	Units
Symbol	Parameter	Conditions	Typical		Limit	(Limits)
	RAMETERS			(Notes 3, 4)	(Note 5)	
	NPN Switch	$V_{COMP} = 2.0V$	4.3		1	A
	Current Limit	COMP - 2.0V	4.5	3.7/ <b>3.0</b>	3.7/ <b>3.0</b>	A(min)
				5.3/ <b>6.0</b>	5.3/ <b>6.0</b>	A(max)
Specificati	ions with standard type fa	tics—LM1577-ADJ, L ce are for $T_J = 25^{\circ}C$ , and those in b $V_{IN} = 5V$ , $V_{FEEDBACK} = V_{REF}$ , and I	old type fac		Operating Te	mperature
				LM1577-ADJ	LM2577-ADJ	Units
Symbol	Parameter	Conditions	Typical	Limit	Limit	(Limits)
•,			.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	(Notes 3, 4)	(Note 5)	()
SYSTEM PA	ARAMETERS Circuit of Fi	igure 3 (Note 6)			, , , , , , , , , , , , , , , , , , ,	
V <sub>OUT</sub>	Output Voltage	$V_{IN} = 5V$ to 10V	12.0			V
-		$I_{LOAD} = 100 \text{ mA to } 800 \text{ mA}$		11.60/ <b>11.40</b>	11.60/ <b>11.40</b>	V(min)
		(Note 3)		12.40/ <b>12.60</b>	12.40/ <b>12.60</b>	V(max)
۷ <sub>out</sub> /	Line Regulation	V <sub>IN</sub> = 3.5V to 10V	20			mV
ΔV <sub>IN</sub>	_	$I_{LOAD} = 300 \text{ mA}$		50/ <b>100</b>	50/ <b>100</b>	mV(max)
ΔV <sub>OUT</sub> /	Load Regulation	$V_{IN} = 5V$	20			mV
∆I <sub>load</sub>		$I_{LOAD} = 100 \text{ mA to } 800 \text{ mA}$		50/ <b>100</b>	50/ <b>100</b>	mV(max)
1	Efficiency	$V_{IN} = 5V, I_{LOAD} = 800 \text{ mA}$	80			%
DEVICE PA	RAMETERS					
S	Input Supply Current	$V_{\text{FEEDBACK}} = 1.5V$ (Switch Off)	7.5			mA
				10.0/ <b>14.0</b>	10.0/ <b>14.0</b>	mA(max)
		I <sub>SWITCH</sub> = 2.0A	25			mA
		V <sub>COMP</sub> = 2.0V (Max Duty Cycle)		50/ <b>85</b>	50/ <b>85</b>	mA(max)
V <sub>UV</sub>	Input Supply	I <sub>SWITCH</sub> = 100 mA	2.90			V
	Undervoltage Lockout			2.70/ <b>2.65</b>	2.70/ <b>2.65</b>	V(min)
				3.10/ <b>3.15</b>	3.10/ <b>3.15</b>	V(max)
0	Oscillator Frequency	Measured at Switch Pin	52			kHz
		I <sub>SWITCH</sub> = 100 mA		48/ <b>42</b>	48/ <b>42</b>	kHz(min)
				56/ <b>62</b>	56/ <b>62</b>	kHz(max)
V <sub>REF</sub>	Reference	Measured at Feedback Pin	1			V
	Voltage	$V_{IN} = 3.5V$ to 40V	1.230	1.214/ <b>1.206</b>	1.214/ <b>1.206</b>	V(min)
	Defense a Maltana	$V_{COMP} = 1.0V$	0.5	1.246/ <b>1.254</b>	1.246/ <b>1.254</b>	V(max)
V <sub>REF</sub> /	Reference Voltage	$V_{IN} = 3.5V$ to 40V	0.5			mV
ΔV <sub>IN</sub>	Line Regulation	1 OV	100			
В	Error Amp	$V_{COMP} = 1.0V$	100	200/000	200/000	nA
2	Input Bias Current	I <sub>COMP</sub> = -30 μA to +30 μA	2700	300/ <b>800</b>	300/ <b>800</b>	nA(max)
З <sub>м</sub>	Error Amp Transconductance		3700	2400/ <b>1600</b>	2400/ <b>1600</b>	µmho µmho(min
	Tansconductance	$V_{COMP} = 1.0V$		2400/ <b>1600</b> 4800/ <b>5800</b>	4800/ <b>5800</b>	• •
AVOL	Error Amp	V <sub>COMP</sub> = 1.1V to 1.9V	800	4000/ <b>3000</b>	4000/ <b>3000</b>	µmho(ma) V/V
		$V_{COMP} = 1.1V U 1.9V$	1 000	1	ı	V/V

## Electrical Characteristics—LM1577-ADJ, LM2577-ADJ (Continued)

Specifications with standard type face are for  $T_J = 25^{\circ}C$ , and those in **bold type face** apply over full **Operating Temperature Range**. Unless otherwise specified,  $V_{IN} = 5V$ ,  $V_{FEEDBACK} = V_{REF}$ , and  $I_{SWITCH} = 0$ .

				LM1577-ADJ	LM2577-ADJ	Units
Symbol	Parameter	Conditions	Typical	Limit	Limit	(Limits)
				(Notes 3, 4)	(Note 5)	
DEVICE PA	RAMETERS					
	Error Amplifier	Upper Limit	2.4			V
	Output Swing	$V_{\text{FEEDBACK}} = 1.0V$		2.2/ <b>2.0</b>	2.2/ <b>2.0</b>	V(min)
		Lower Limit	0.3			V
		$V_{\text{FEEDBACK}} = 1.5V$		0.40/ <b>0.55</b>	0.40/ <b>0.55</b>	V(max)
	Error Amp	$V_{\text{FEEDBACK}} = 1.0V \text{ to } 1.5V$	±200			μA
	Output Current	$V_{COMP} = 1.0V$		±130/ <b>±90</b>	±130/ <b>±90</b>	μA(min)
				±300/ <b>±400</b>	±300/ <b>±400</b>	µA(max)
I <sub>SS</sub>	Soft Start Current	V <sub>FEEDBACK</sub> = 1.0V	5.0			μA
		$V_{COMP} = 0V$		2.5/ <b>1.5</b>	2.5/ <b>1.5</b>	μA(min)
				7.5/ <b>9.5</b>	7.5/ <b>9.5</b>	µA(max)
D	Maximum Duty Cycle	$V_{COMP} = 1.5V$	95			%
		I <sub>SWITCH</sub> = 100 mA		93/ <b>90</b>	93/ <b>90</b>	%(min)
Δl <sub>switch</sub> /	Switch		12.5			A/V
$\Delta V_{COMP}$	Transconductance					
IL	Switch Leakage	V <sub>SWITCH</sub> = 65V	10			μA
	Current	V <sub>FEEDBACK</sub> = 1.5V (Switch Off)		300/ <b>600</b>	300/ <b>600</b>	µA(max)
V <sub>SAT</sub>	Switch Saturation	I <sub>SWITCH</sub> = 2.0A	0.5			V
	Voltage	V <sub>COMP</sub> = 2.0V (Max Duty Cycle)		0.7/ <b>0.9</b>	0.7/ <b>0.9</b>	V(max)
	NPN Switch	$V_{COMP} = 2.0V$	4.3			A
	Current Limit			3.7/ <b>3.0</b>	3.7/ <b>3.0</b>	A(min)
				5.3/ <b>6.0</b>	5.3/ <b>6.0</b>	A(max)
THERMAL	PARAMETERS (All Vers	ions)	1	•	L1	
θ <sub>JA</sub>	Thermal Resistance	K Package, Junction to Ambient	35			
$\theta_{\text{JC}}$		K Package, Junction to Case	1.5			
θ <sub>JA</sub>	1	T Package, Junction to Ambient	65			
θ <sub>JC</sub>		T Package, Junction to Case	2			
θ <sub>JA</sub>	1	N Package, Junction to	85			°044
		Ambient (Note 8)				°C/W
θ <sub>JA</sub>	1	M Package, Junction	100			
		to Ambient (Note 8)				
θ <sub>JA</sub>		S Package, Junction to	37			
0.1		Ambient (Note 9)				

Note 1: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating ratings indicate conditions the device is intended to be functional, but device parameter specifications may not be guaranteed under these conditions. For guaranteed specifications and test conditions, see the Electrical Characteristics.

Note 2: Due to timing considerations of the LM1577/LM2577 current limit circuit, output current cannot be internally limited when the LM1577/LM2577 is used as a step-up regulator. To prevent damage to the switch, its current must be externally limited to 6.0A. However, output current is internally limited when the LM1577/LM2577 is used as a flyback or forward converter regulator in accordance to the Application Hints.

Note 3: All limits guaranteed at room temperature (standard type face) and at temperature extremes (boldface type). All limits are used to calculate Outgoing Quality Level, and are 100% production tested.

**Note 4:** A military RETS electrical test specification is available on request. At the time of printing, the LM1577K-12/883, LM1577K-15/883, and LM1577K-ADJ/883 RETS specifications complied fully with the boldface limits in these columns. The LM1577K-12/883, LM1577K-15/883, and LM1577K-ADJ/883 may also be procured to Standard Military Drawing specifications.

Note 5: All limits guaranteed at room temperature (standard type face) and at temperature extremes (boldface type). All room temperature limits are 100% production tested. All limits at temperature extremes are guaranteed via correlation using standard Statistical Quality Control (SQC) methods.

Note 6: External components such as the diode, inductor, input and output capacitors can affect switching regulator performance. When the LM1577/LM2577 is used as shown in the Test Circuit, system performance will be as specified by the system parameters.

**Note 7:** A 1.0 M $\Omega$  resistor is connected to the compensation pin (which is the error amplifier's output) to ensure accuracy in measuring A<sub>VOL</sub>. In actual applications, this pin's load resistance should be  $\geq$ 10 M $\Omega$ , resulting in A<sub>VOL</sub> that is typically twice the guaranteed minimum limit.

## Electrical Characteristics—LM1577-ADJ, LM2577-ADJ (Continued)

Note 8: Junction to ambient thermal resistance with approximately 1 square inch of pc board copper surrounding the leads. Additional copper area will lower thermal resistance further. See thermal model in "Switchers Made Simple" software.

**Note 9:** If the TO-263 package is used, the thermal resistance can be reduced by increasing the PC board copper area thermally connected to the package. Using 0.5 square inches of copper area,  $\theta_{JA}$  is 50°C/W; with 1 square inch of copper area,  $\theta_{JA}$  is 37°C/W; and with 1.6 or more square inches of copper area,  $\theta_{JA}$  is 30°C/W.







80

60

-50 -25 0

25 50 75 100 125 150

01146844

TEMPERATURE (°C)



## Typical Performance Characteristics (Continued)









## LM1577-12, LM2577-12 Test Circuit



**Note:** Pin numbers shown are for TO-220 (T) package

FIGURE 1. Circuit Used to Specify System Parameters for 12V Versions

## LM1577-15, LM2577-15 Test Circuit



Note: Pin numbers shown are for TO-220 (T) package



## LM1577-ADJ, LM2577-ADJ Test Circuit



FIGURE 3. Circuit Used to Specify System Parameters for ADJ Versions

## **Application Hints**



Note: Pin numbers shown are for TO-220 (T) package \*Resistors are internal to LM1577/LM2577 for 12V and 15V versions.



#### STEP-UP (BOOST) REGULATOR

*Figure 4* shows the LM1577-ADJ/LM2577-ADJ used as a Step-Up Regulator. This is a switching regulator used for producing an output voltage greater than the input supply voltage. The LM1577-12/LM2577-12 and LM1577-15/LM2577-15 can also be used for step-up regulators with 12V or 15V outputs (respectively), by tying the feedback pin directly to the regulator output.

A basic explanation of how it works is as follows. The LM1577/LM2577 turns its output switch on and off at a frequency of 52 kHz, and this creates energy in the inductor (L). When the NPN switch turns on, the inductor current charges up at a rate of  $V_{\rm IN}/L$ , storing current in the inductor. When the switch turns off, the lower end of the inductor flies above V<sub>IN</sub>, discharging its current through diode (D) into the output capacitor ( $C_{OUT}$ ) at a rate of ( $V_{OUT} - V_{IN}$ )/L. Thus, energy stored in the inductor during the switch on time is transferred to the output during the switch off time. The output voltage is controlled by the amount of energy transferred which, in turn, is controlled by modulating the peak inductor current. This is done by feeding back a portion of the output voltage to the error amp, which amplifies the difference between the feedback voltage and a 1.230V reference. The error amp output voltage is compared to a voltage proportional to the switch current (i.e., inductor current during the switch on time).

The comparator terminates the switch on time when the two voltages are equal, thereby controlling the peak switch current to maintain a constant output voltage.

Voltage and current waveforms for this circuit are shown in *Figure 5*, and formulas for calculating them are given in *Figure 6*.





Duty Cycle	D	$\frac{V_{\text{OUT}} + V_{\text{F}} - V_{\text{IN}}}{V_{\text{OUT}} + V_{\text{F}} - V_{\text{SAT}}} \approx \frac{V_{\text{OUT}} - V_{\text{IN}}}{V_{\text{OUT}}}$
Average Inductor Current	I <sub>IND(AVE)</sub>	l <sub>LOAD</sub> 1 — D
Inductor Current Ripple	Δl <sub>ind</sub>	$\frac{V_{\text{IN}} - V_{\text{SAT}}}{L} \frac{D}{52,000}$
Peak Inductor Current	I <sub>IND(PK)</sub>	$\frac{I_{LOAD(max)}}{1 - D_{(max)}} + \frac{\Delta I_{IND}}{2}$
Peak Switch Current	I <sub>SW(PK)</sub>	$\frac{I_{LOAD(max)}}{1 - D_{(max)}} + \frac{\Delta I_{IND}}{2}$
Switch Voltage When Off	V <sub>SW(OFF)</sub>	V <sub>OUT</sub> + V <sub>F</sub>
Diode Reverse Voltage	V <sub>R</sub>	V <sub>OUT</sub> – V <sub>SAT</sub>
Average Diode Current	I <sub>D(AVE)</sub>	I <sub>LOAD</sub>
Peak Diode Current	I <sub>D(PK)</sub>	$\frac{I_{LOAD}}{1-D_{(max)}} + \frac{\Delta I_{IND}}{2}$
Power Dissipation of LM1577/2577	P <sub>D</sub>	$0.25\Omega \left(\frac{I_{LOAD}}{1-D}\right)^2 D + \frac{I_{LOAD} D V_{IN}}{50 (1-D)}$

ILOAD = Output Load Current

#### FIGURE 6. Step-Up Regulator Formulas

#### STEP-UP REGULATOR DESIGN PROCEDURE

The following design procedure can be used to select the appropriate external components for the circuit in *Figure 4*, based on these system requirements.

Given:

V<sub>IN (min)</sub> = Minimum input supply voltage

 $V_{OUT}$  = Regulated output voltage

I<sub>LOAD(max)</sub> = Maximum output load current

Before proceeding any further, determine if the LM1577/ LM2577 can provide these values of  $V_{\rm OUT}$  and  $I_{\rm LOAD(max)}$  when operating with the minimum value of  $V_{\rm IN}$ . The upper limits for  $V_{\rm OUT}$  and  $I_{\rm LOAD(max)}$  are given by the following equations.

$$\label{eq:Vout} \begin{split} V_{OUT} &\leq 60V \\ \text{and} \quad V_{OUT} &\leq 10 ~x ~V_{\text{IN}(\text{min})} \end{split}$$

ЧĿ

$$ext{DAD(max)} \leq rac{2.1 ext{A} imes ext{V}_{ ext{IN(min)}}}{ ext{V}_{ ext{OUT}}}$$

These limits must be greater than or equal to the values specified in this application.

- 1. Inductor Selection (L)
  - A. Voltage Options:
  - 1. For 12V or 15V output

From Figure 7 (for 12V output) or Figure 8 (for 15V output), identify inductor code for region indicated by  $V_{IN (min)}$  and  $I_{LOAD (max)}$ . The shaded region indicates con-

ditions for which the LM1577/LM2577 output switch would be operating beyond its switch current rating. The minimum operating voltage for the LM1577/LM2577 is 3.5V.

From here, proceed to step C.

#### 2. For Adjustable version

#### Preliminary calculations:

The inductor selection is based on the calculation of the following three parameters:

 $D_{(max)}$ , the maximum switch duty cycle (0  $\leq D \leq 0.9$ ):

$$\mathsf{D}_{(\text{max})} = \frac{\mathsf{V}_{\text{OUT}} + \mathsf{V}_{\text{F}} - \mathsf{V}_{\text{IN}(\text{min})}}{\mathsf{V}_{\text{OUT}} + \mathsf{V}_{\text{F}} - 0.6\mathsf{V}}$$

where  $V_F = 0.5V$  for Schottky diodes and 0.8V for fast recovery diodes (typically);

 $E \bullet T$ , the product of volts x time that charges the inductor:

$$\mathsf{E} \bullet \mathsf{T} = \frac{\mathsf{D}_{(\text{max})} (\mathsf{V}_{\text{IN}(\text{min})} - 0.6\mathsf{V}) 10^6}{52,000 \text{ Hz}} \qquad (\mathsf{V} \bullet \mu s)$$

I<sub>IND,DC</sub>, the average inductor current under full load;

$$I_{\text{IND,DC}} = \frac{1.05 \times I_{\text{LOAD(max)}}}{1 - D_{\text{(max)}}}$$

#### B. Identify Inductor Value:

1. From *Figure 9*, identify the inductor code for the region indicated by the intersection of E•T and I<sub>IND,DC</sub>. This code gives the inductor value in microhenries. The L or H prefix signifies whether the inductor is rated for a maximum E•T of 90 V•µs (L) or 250 V•µs (H).

2. If D < 0.85, go on to step C. If D  $\ge$  0.85, then calculate the minimum inductance needed to ensure the switching regulator's stability:

$$L_{MIN} = \frac{6.4 (V_{IN(min)} - 0.6V) (2D_{(max)} - 1)}{1 - D_{(max)}} \quad (\mu H)$$

If  $L_{MIN}$  is smaller than the inductor value found in step B1, go on to step C. Otherwise, the inductor value found in step B1 is too low; an appropriate inductor code should be obtained from the graph as follows:

1. Find the lowest value inductor that is greater than  $L_{MIN}$ . 2. Find where E•T intersects this inductor value to determine if it has an L or H prefix. If E•T intersects both the L and H regions, select the inductor with an H prefix.



FIGURE 7. LM2577-12 Inductor Selection Guide



FIGURE 8. LM2577-15 Inductor Selection Guide

200

150

100

90 80 70

60 50 45

40 35 30

25

20



Note: These charts assume that the inductor ripple current inductor is approximately 20% to 30% of the average inductor current (when the regulator is under full load). Greater ripple current causes higher peak switch currents and greater output ripple voltage; lower ripple current is achieved with larger-value inductors. The factor of 20 to 30% is chosen as a convenient balance between the two extremes.

#### FIGURE 9. LM1577-ADJ/LM2577-ADJ Inductor Selection Graph

C. Select an inductor from the table of Figure 10 which cross-references the inductor codes to the part numbers of three different manufacturers. Complete specifications for these inductors are available from the respective manufacturers. The inductors listed in this table have the following characteristics:

*AIE:* ferrite, pot-core inductors; Benefits of this type are low electro-magnetic interference (EMI), small physical size, and very low power dissipation (core loss). Be careful not to operate these inductors too far beyond their maximum ratings for E•T and peak current, as this will saturate the core.

*Pulse:* powdered iron, toroid core inductors; Benefits are low EMI and ability to withstand E•T and peak current above rated value better than ferrite cores.

*Renco:* ferrite, bobbin-core inductors; Benefits are low cost and best ability to withstand E•T and peak current above rated value. Be aware that these inductors generate more EMI than the other types, and this may interfere with signals sensitive to noise.

Inductor	Manufa	cturer's Part Nu	Imber
Code	Schott	Pulse	Renco
L47	67126980	PE - 53112	RL2442
L68	67126990	PE - 92114	RL2443
L100	67127000	PE - 92108	RL2444
L150	67127010	PE - 53113	RL1954
L220	67127020	PE - 52626	RL1953
L330	67127030	PE - 52627	RL1952
L470	67127040	PE - 53114	RL1951
L680	67127050	PE - 52629	RL1950
H150	67127060	PE - 53115	RL2445
H220	67127070	PE - 53116	RL2446
H330	67127080	PE - 53117	RL2447
H470	67127090	PE - 53118	RL1961
H680	67127100	PE - 53119	RL1960
H1000	67127110	PE - 53120	RL1959
H1500	67127120	PE - 53121	RL1958
H2200	67127130	PE - 53122	RL2448

Schott Corp., (612) 475-1173

1000 Parkers Lake Rd., Wayzata, MN 55391 Pulse Engineering, (619) 268-2400 P.O. Box 12235, San Diego, CA 92112 Renco Electronics Inc., (516) 586-5566

60 Jeffryn Blvd. East, Deer Park, NY 11729

#### FIGURE 10. Table of Standardized Inductors and Manufacturer's Part Numbers

#### 2. Compensation Network (R<sub>C</sub>, C<sub>C</sub>) and Output Capacitor (C<sub>OUT</sub>) Selection

 $R_{\rm C}$  and  $C_{\rm C}$  form a pole-zero compensation network that stabilizes the regulator. The values of  $R_C$  and  $C_C$  are mainly dependant on the regulator voltage gain, ILOAD(max), L and  $C_{OUT}$ . The following procedure calculates values for  $R_C$ ,  $C_C$ , and COUT that ensure regulator stability. Be aware that this procedure doesn't necessarily result in R<sub>C</sub> and C<sub>C</sub> that provide optimum compensation. In order to guarantee optimum compensation, one of the standard procedures for testing loop stability must be used, such as measuring  $V_{OUT}$  transient response when pulsing ILOAD (see Figure 15).

A. First, calculate the maximum value for R<sub>C</sub>.

$$\text{R}_{C} \leq \frac{750 \times \text{I}_{\text{LOAD}(\text{max})} \times \text{V}_{\text{OUT}}^{2}}{\text{V}_{\text{IN}(\text{min})}^{2}}$$

Select a resistor less than or equal to this value, and it should also be no greater than 3 k $\Omega$ .

B. Calculate the minimum value for COUT using the following two equations. 

$$C_{OUT} \ge \frac{0.19 \times L \times R_C \times I_{LOAD(max)}}{V_{IN(min)} \times V_{OUT}}$$

and

$$C_{OUT} \geq \frac{V_{IN(min)} \times R_C \times (V_{IN(min)} + (3.74 \times 10^5 \times L))}{487,800 \times V_{OUT}^3}$$

The larger of these two values is the minimum value that ensures stability.

C. Calculate the minimum value of  $C_C$ .

$$C_{C} \geq \frac{58.5 \times V_{OUT}^{2} \times C_{OUT}}{R_{C}^{2} \times V_{IN(min)}}$$

The compensation capacitor is also part of the soft start circuitry. When power to the regulator is turned on, the switch duty cycle is allowed to rise at a rate controlled by this capacitor (with no control on the duty cycle, it would immediately rise to 90%, drawing huge currents from the input power supply). In order to operate properly, the soft start circuit requires  $C_C \ge 0.22 \ \mu F$ .

The value of the output filter capacitor is normally large enough to require the use of aluminum electrolytic capacitors. Figure 11 lists several different types that are recommended for switching regulators, and the following parameters are used to select the proper capacitor.

Working Voltage (WVDC): Choose a capacitor with a working voltage at least 20% higher than the regulator output voltage.

Ripple Current: This is the maximum RMS value of current that charges the capacitor during each switching cycle. For step-up and flyback regulators, the formula for ripple current is

$$\mathsf{I}_{\mathsf{RIPPLE}(\mathsf{RMS})} = \frac{\mathsf{I}_{\mathsf{LOAD}(\mathsf{max})} \times \mathsf{D}_{(\mathsf{max})}}{1 - \mathsf{D}_{(\mathsf{max})}}$$

Choose a capacitor that is rated at least 50% higher than this value at 52 kHz.

Equivalent Series Resistance (ESR) : This is the primary cause of output ripple voltage, and it also affects the values of R<sub>C</sub> and C<sub>C</sub> needed to stabilize the regulator. As a result, the preceding calculations for  $C_C$  and  $R_C$  are only valid if ESR doesn't exceed the maximum value specified by the following equations.

$$ESR \leq \frac{0.01 \times V_{OUT}}{I_{RIPPLE(P-P)}} \text{ and } \leq \frac{8.7 \times (10) - 3 \times V_{IN}}{I_{LOAD(max)}}$$

where

$$\mathsf{I}_{\mathsf{RIPPLE}(\mathsf{P}-\mathsf{P})} = rac{1.15 imes \mathsf{I}_{\mathsf{LOAD}(\mathsf{max})}}{1 - \mathsf{D}_{(\mathsf{max})}}$$

Select a capacitor with ESR, at 52 kHz, that is less than or equal to the lower value calculated. Most electrolytic capacitors specify ESR at 120 Hz which is 15% to 30% higher than at 52 kHz. Also, be aware that ESR increases by a factor of 2 when operating at -20°C.

In general, low values of ESR are achieved by using large value capacitors (C  $\geq$  470 µF), and capacitors with high WVDC, or by paralleling smaller-value capacitors.

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#### 3. Output Voltage Selection (R1 and R2)

This section is for applications using the LM1577-ADJ/ LM2577-ADJ. Skip this section if the LM1577-12/LM2577-12 or LM1577-15/LM2577-15 is being used.

With the LM1577-ADJ/LM2577-ADJ, the output voltage is given by

$$V_{OUT} = 1.23V (1 + R1/R2)$$

Resistors R1 and R2 divide the output down so it can be compared with the LM1577-ADJ/LM2577-ADJ internal 1.23V reference. For a given desired output voltage  $V_{OUT}$ , select R1 and R2 so that

$$\frac{\mathrm{R1}}{\mathrm{R2}} = \frac{\mathrm{V}_{\mathrm{OUT}}}{\mathrm{1.23V}} - 1$$

#### 4. Input Capacitor Selection (C<sub>IN</sub>)

The switching action in the step-up regulator causes a triangular ripple current to be drawn from the supply source. This in turn causes noise to appear on the supply voltage. For proper operation of the LM1577, the input voltage should be decoupled. Bypassing the Input Voltage pin directly to ground with a good quality, low ESR, 0.1  $\mu$ F capacitor (leads as short as possible) is normally sufficient.

Cornell Dublier — Types 239, 250, 251,	UFT,
300, or 350	-
P.O. Box 128, Pickens, SC 29671	
(803) 878-6311	
Nichicon — Types PF, PX, or PZ	
927 East Parkway,	
Schaumburg, IL 60173	
(708) 843-7500	
<b>Sprague</b> — Types 672D, 673D, or 674D	
Box 1, Sprague Road,	
Lansing, NC 28643	
(919) 384-2551	
United Chemi-Con — Types LX, SXF, o	r SXJ
9801 West Higgins Road,	
Rosemont, IL 60018	
(708) 696-2000	

FIGURE 11. Aluminum Electrolytic Capacitors Recommended for Switching Regulators If the LM1577 is located far from the supply source filter capacitors, an additional large electrolytic capacitor (e.g. 47  $\mu$ F) is often required.

#### 5. Diode Selection (D)

The switching diode used in the boost regulator must withstand a reverse voltage equal to the circuit output voltage, and must conduct the peak output current of the LM2577. A suitable diode must have a minimum reverse breakdown voltage greater than the circuit output voltage, and should be rated for average and peak current greater than I<sub>LOAD(max)</sub> and I<sub>D(PK)</sub>. Schottky barrier diodes are often favored for use in switching regulators. Their low forward voltage drop allows higher regulator efficiency than if a (less expensive) fast recovery diode was used. See *Figure 12* for recommended part numbers and voltage ratings of 1A and 3A diodes.

Vout	Schottky		Fast Recovery	
(max)	1A	3A	1 <b>A</b>	3A
20V	1N5817	1N5820		
	MBR120P	MBR320P		
	1N5818	1N5821		
30V	MBR130P	MBR330P		
	11DQ03	31DQ03		
	1N5819	1N5822		
40V	MBR140P	MBR340P		
	11DQ04	31DQ04		
	MBR150	MBR350	1N4933	
50V	11DQ05	31DQ05	MUR105	
			1N4934	MR851
100V			HER102	30DL1
			MUR110	MR831
			10DL1	HER302

FIGURE 12. Diode Selection Chart

#### BOOST REGULATOR CIRCUIT EXAMPLE

By adding a few external components (as shown in *Figure 13*), the LM2577 can be used to produce a regulated output voltage that is greater than the applied input voltage. Typical performance of this regulator is shown in *Figure 14* and *Figure 15*. The switching waveforms observed during the operation of this circuit are shown in *Figure 16*.



#### FLYBACK REGULATOR

A Flyback regulator can produce single or multiple output voltages that are lower or greater than the input supply voltage. *Figure 18* shows the LM1577/LM2577 used as a flyback regulator with positive and negative regulated outputs. Its operation is similar to a step-up regulator, except the output switch contols the primary current of a flyback transformer. Note that the primary and secondary windings are out of phase, so no current flows through secondary when current flows through the primary. This allows the primary to charge up the transformer core when the switch is on. When the switch turns off, the core discharges by sending current through the secondary, and this produces voltage at the outputs. The output voltages are controlled by adjusting the peak primary current, as described in the step-up regulator section.

Voltage and current waveforms for this circuit are shown in *Figure 17*, and formulas for calculating them are given in *Figure 19*.

#### FLYBACK REGULATOR DESIGN PROCEDURE

#### 1. Transformer Selection

A family of standardized flyback transformers is available for creating flyback regulators that produce dual output voltages, from  $\pm 10V$  to  $\pm 15V$ , as shown in *Figure 18. Figure 20* lists these transformers with the input voltage, output voltages and maximum load current they are designed for.

## 2. Compensation Network (C<sub>c</sub>, R<sub>c</sub>) and Output Capacitor (C<sub>OUT</sub>) Selection

As explained in the Step-Up Regulator Design Procedure, C<sub>C</sub>, R<sub>C</sub> and C<sub>OUT</sub> must be selected as a group. The following procedure is for a dual output flyback regulator with equal turns ratios for each secondary (i.e., both output voltages have the same magnitude). The equations can be used for a single output regulator by changing  $\Sigma I_{LOAD(max)}$  to  $I_{LOAD(max)}$  in the following equations.

A. First, calculate the maximum value for  $\mathbf{R}_{\mathbf{C}}$ 

$$R_C \leq \frac{750 \times \Sigma I_{LOAD(max)} \times (15V + V_{IN(min)}N)^2}{V_{IN(min)}^2}$$

Where  $\Sigma I_{\text{LOAD}(max)}$  is the sum of the load current (magnitude) required from both outputs. Select a resistor less than or equal to this value, and no greater than 3 k $\Omega$ .

B. Calculate the minimum value for  $\Sigma C_{OUT}$  (sum of  $C_{OUT}$  at both outputs) using the following two equations.

$$C_{OUT} \geq \frac{0.19 \times R_{C} \times L_{P} \times \Sigma I_{LOAD(max)}}{15V \times V_{IN(min)}}$$

and

$$C_{OUT} \ge \frac{V_{IN(min)} \times R_C \times N^2 \times (V_{IN(min)} + (3.74 \times 10^5 \times L_P))}{487,800 \times (15V)^2 \times (15V + V_{IN(min)} \times N)}$$

The larger of these two values must be used to ensure regulator stability.







Duty Cycle	D	$\frac{\frac{V_{OUT} + V_{F}}{N (V_{IN} - V_{SAT}) + V_{OUT} + V_{F}}}{\frac{V_{OUT}}{N (V_{IN}) + V_{OUT}}} \approx$
Primary Current Variation	Δl <sub>P</sub>	$\frac{\text{D} (\text{V}_{\text{IN}} - \text{V}_{\text{SAT}})}{\text{L}_{\text{P}} \times 52,000}$
Peak Primary Current	I <sub>P(PK)</sub>	$\frac{N}{\eta} \times \frac{\Sigma I_{LOAD}}{1-D} + \frac{\Delta I_{PK}}{2}$
Switch Voltage when Off	V <sub>SW(OFF)</sub>	$V_{IN} + \frac{V_{OUT} + V_F}{N}$
Diode Reverse Voltage	V <sub>R</sub>	$V_{OUT}^+ N (V_{IN}^- V_{SAT})$
Average Diode Current	I <sub>D(AVE)</sub>	I <sub>LOAD</sub>
Peak Diode Current	I <sub>D(РК)</sub>	$\frac{I_{LOAD}}{1-D} + \frac{\Delta I_{IND}}{2}$
Short Circuit Diode Current		$\approx \frac{6A}{N}$
Power Dissipation of LM1577/LM2577	P <sub>D</sub>	$0.25\Omega \left(\frac{N \Sigma I_{LOAD}}{1 - D}\right)^2 + \frac{N I_{LOAD}D}{50 (1 - D)} V_{IN}$

 $N = Transformer Turns Ratio = \frac{number of secondary turns}{number of primary turns}$ 

 $\eta$  = Transformer Efficiency *(typically 0.95)*  $\Sigma I_{LOAD} = |+I_{LOAD}|+|-I_{LOAD}|$ 





C. Calculate the minimum value of  $C_C$ 

$$C_{C} \geq \frac{58.5 \times C_{OUT} \times V_{OUT} \times (V_{OUT} + (V_{IN(min)} \times N))}{R_{C}^{2} \times V_{IN(min)} \times N}$$

D. Calculate the maximum ESR of the  $+V_{\rm OUT}$  and  $-V_{\rm OUT}$  output capacitors in parallel.

$$\text{ESR} + \|\text{ESR}_{-} \leq \frac{8.7 \times 10^{-3} \times \text{V}_{\text{IN}(\text{min})} \times \text{V}_{\text{OUT}} \times \text{N}}{\Sigma \text{I}_{\text{LOAD}(\text{max})} \times (\text{V}_{\text{OUT}}^{+} (\text{V}_{\text{IN}(\text{min})} \times \text{N}))}$$

This formula can also be used to calculate the maximum ESR of a single output regulator.

At this point, refer to this same section in the **Step-Up Regulator Design Procedure** for more information regarding the selection of  $C_{OUT}$ .

#### 3. Output Voltage Selection

This section is for applications using the LM1577-ADJ/ LM2577-ADJ. Skip this section if the LM1577-12/LM2577-12 or LM1577-15/LM2577-15 is being used.

With the LM1577-ADJ/LM2577-ADJ, the output voltage is given by

$$V_{OUT} = 1.23V (1 + R1/R2)$$

Resistors R1 and R2 divide the output voltage down so it can be compared with the LM1577-ADJ/LM2577-ADJ internal 1.23V reference. For a desired output voltage  $V_{OUT}$ , select R1 and R2 so that

$$\frac{\mathrm{R1}}{\mathrm{R2}} = \frac{\mathrm{V}_{\mathrm{OUT}}}{\mathrm{1.23V}} - 1$$

#### 4. Diode Selection

The switching diode in a flyback converter must withstand the reverse voltage specified by the following equation.

$$V_{R} = V_{OUT} + \frac{V_{IN}}{N}$$

A suitable diode must have a reverse voltage rating greater than this. In addition it must be rated for more than the average and peak diode currents listed in *Figure 19*.

#### 5. Input Capacitor Selection

The primary of a flyback transformer draws discontinuous pulses of current from the input supply. As a result, a flyback regulator generates more noise at the input supply than a

step-up regulator, and this requires a larger bypass capacitor to decouple the LM1577/LM2577  $V_{\rm IN}$  pin from this noise. For most applications, a low ESR, 1.0  $\mu F$  cap will be sufficient, if it is connected very close to the  $V_{\rm IN}$  and Ground pins.

1	Fransformer	Input	Dual	Maximum
	Туре	Voltage	Output	Output
			Voltage	Current
	L <sub>P</sub> = 100 μH	5V	±10V	325 mA
1	N = 1	5V	±12V	275 mA
		5V	±15V	225 mA
		10V	±10V	700 mA
		10V	±12V	575 mA
2	L <sub>P</sub> = 200 μH	10V	±15V	500 mA
	N = 0.5	12V	±10V	800 mA
		12V	±12V	700 mA
		12V	±15V	575 mA
3	L <sub>P</sub> = 250 μH	15V	±10V	900 mA
	N = 0.5	15V	±12V	825 mA
		15V	±15V	700 mA

Transformer	Manufacturers' Part Numbers			
Туре	AIE	Pulse	Renco	
1	326-0637	PE-65300	RL-2580	
2	330-0202	PE-65301	RL-2581	
3	330-0203	PE-65302	RL-2582	

FIGURE 20. Flyback Transformer Selection Guide

In addition to this bypass cap, a larger capacitor ( $\geq$  47 µF) should be used where the flyback transformer connects to the input supply. This will attenuate noise which may interfere with other circuits connected to the same input supply voltage.

#### 6. Snubber Circuit

A "snubber" circuit is required when operating from input voltages greater than 10V, or when using a transformer with  $L_P \ge 200 \ \mu$ H. This circuit clamps a voltage spike from the transformer primary that occurs immediately after the output switch turns off. Without it, the switch voltage may exceed the 65V maximum rating. As shown in *Figure 21*, the snub-

ber consists of a fast recovery diode, and a parallel RC. The RC values are selected for switch clamp voltage (V<sub>CLAMP</sub>) that is 5V to 10V greater than V<sub>SW(OFF)</sub>. Use the following equations to calculate R and C;

$$\begin{split} & \mathsf{C} \geq \frac{0.02 \times \mathsf{L}_{\mathsf{P}} \times \mathsf{I}_{\mathsf{P}(\mathsf{PK})}^2}{\left(\mathsf{V}_{\mathsf{CLAMP}}\right)^2 - (\mathsf{VSW}_{(\mathsf{OFF})})^2} \\ & \mathsf{R} \leq \left(\frac{\mathsf{V}_{\mathsf{CLAMP}} + \mathsf{V}_{\mathsf{SW}(\mathsf{OFF})} - \mathsf{V}_{\mathsf{IN}}}{2}\right)^2 \times \left(\frac{19.2 \times 10^{-4}}{\mathsf{L}_{\mathsf{P}} \times \mathsf{I}_{\mathsf{P}(\mathsf{PK})}^2}\right) \end{split}$$

Power dissipation (and power rating) of the resistor is;

$$\mathsf{P} = \left(\frac{\mathsf{V}_{\mathsf{CLAMP}} + \mathsf{V}_{\mathsf{SW}(\mathsf{OFF})} - \mathsf{V}_{\mathsf{IN}}}{2}\right)^2 / \mathsf{R}$$

The fast recovery diode must have a reverse voltage rating greater than  $V_{\rm CLAMP}.$ 



FIGURE 21. Snubber Circuit

#### FLYBACK REGULATOR CIRCUIT EXAMPLE

The circuit of *Figure 22* produces  $\pm 15V$  (at 225 mA each) from a single 5V input. The output regulation of this circuit is shown in *Figure 23* and *Figure 25*, while the load transient response is shown in *Figure 24* and *Figure 26*. Switching waveforms seen in this circuit are shown in *Figure 27*.



T1 = Pulse Engineering, PE-65300 D1, D2 = 1N5821

#### FIGURE 22. Flyback Regulator Easily Provides Dual Outputs







A: Output Voltage Change, 100 mV/div B: Output Current, 100 mA/div Horizontal: 10 ms/div

> FIGURE 24. Load Transient Response of Flyback Regulator of *Figure 22*, +15V Output



## Physical Dimensions inches (millimeters) unless otherwise noted







TO-220, Bent Staggered Leads (T) Order Number LM2577T-12 Flow LB03, LM2577T-15 Flow LB03, or LM2577T-ADJ Flow LB03 NS Package Number T05D



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